

GSHPA Thermal Pile Standard

Ground Source Heat Pump Association
Technical Seminar

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Wednesday 16 November 2011
Homerton College, Cambridge University

ARUP

Thermal Pile Standard – sub committee

- **Duncan Nicholson** **Arup** **(Chair)**
- **Nic Wincott** **NeoEnergy**
- **Peter Smith** **Cementation**
- **Tony Amis** **GIL**
- **Chris Wood** **Bullivant /**
- **Kenichi Soga** **Cambridge University**
- **Fleur Loveridge** **Southampton University**
- **Jake Salisbury** **GSHPA -** **(Secretary)**

GSHPA -Thermal Pile Standard overview

■ Contents List

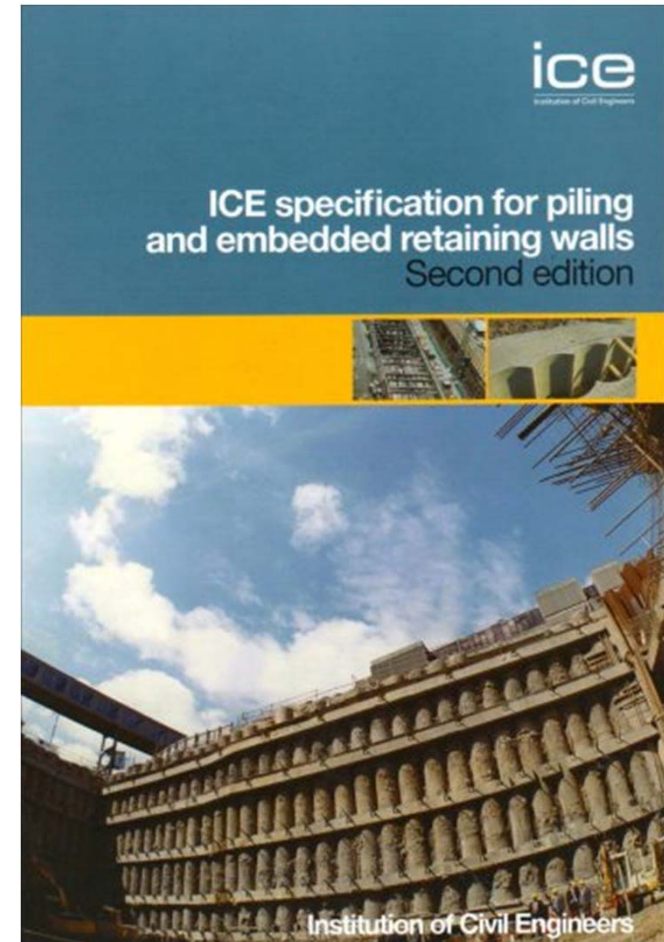
- Sec 1 Preamble (as in the Vertical Borehole Standard)
- Sec 2 Regulations and governments (as VBS)
- Sec 3 **Contractual setup**
- Sec 4 Training requirements (**Link with FPS for piles**)
- Sec 5 **Design**
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- Sec 8 Pipe Jointing (as VBS)
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- Sec 13 Thermal Transfer fluids (as VBS) – **High loop temps – use water as Europe?**
- Sec 14 Design drawings
- Sec 15 **Monitoring and checking**
- Sec 16 Alterations

■ Appendices

- A Design – Geotechnical design issues
- B Thermal response – Effect of large diameter piles
- C Thermal pile concrete – Concrete thermal conductivity
- E Loops Installation – Methods and scratching

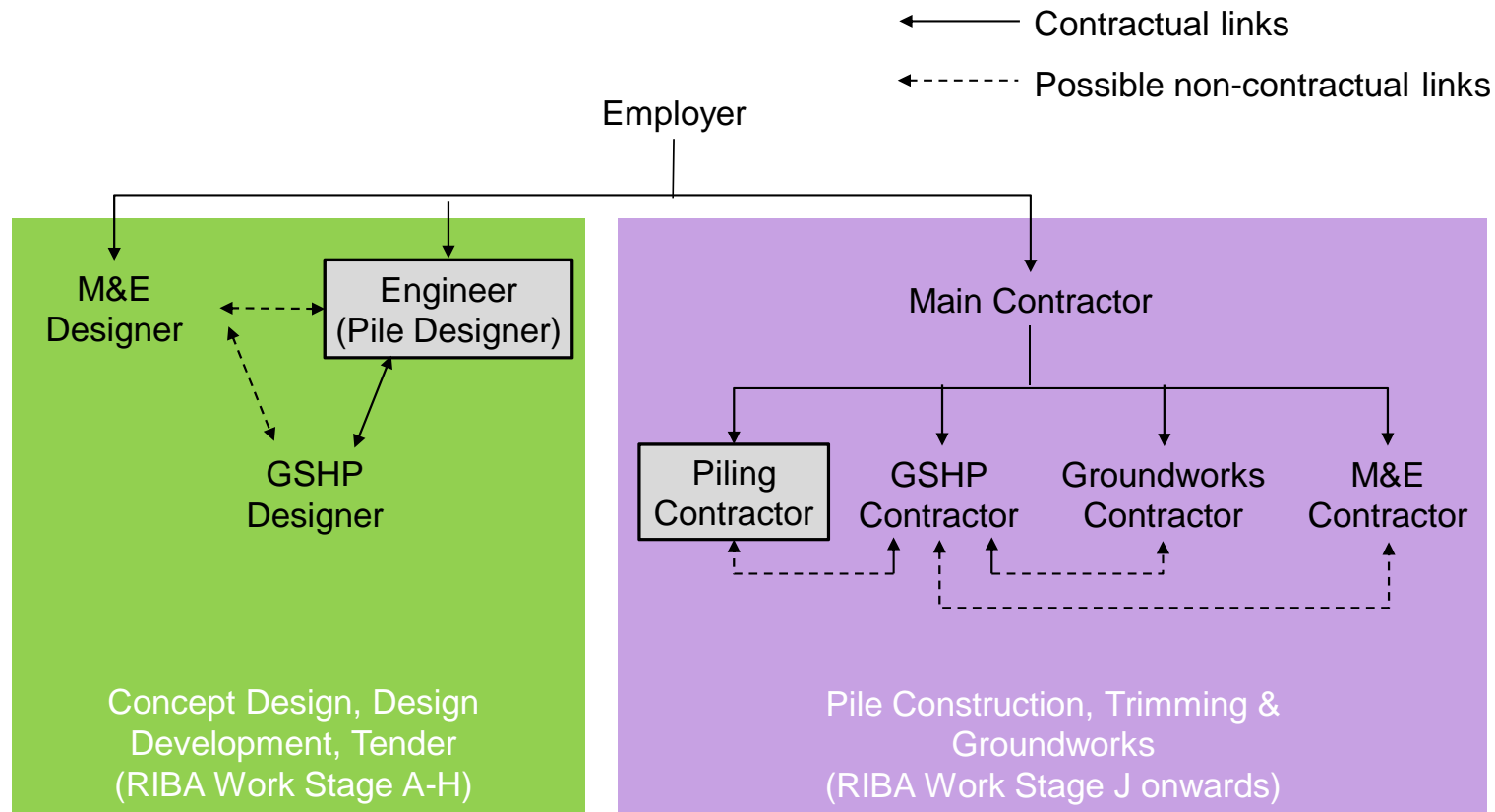
Section 3 Contractual responsibilities

- **Many parties results in division of responsibilities.**
- **ICE Specification for Piling and Embedded Retaining Walls (SPERW) is the starting point**
 - “Engineer” design
 - “Contractor” design
 - Standardise terms



Contractual responsibilities

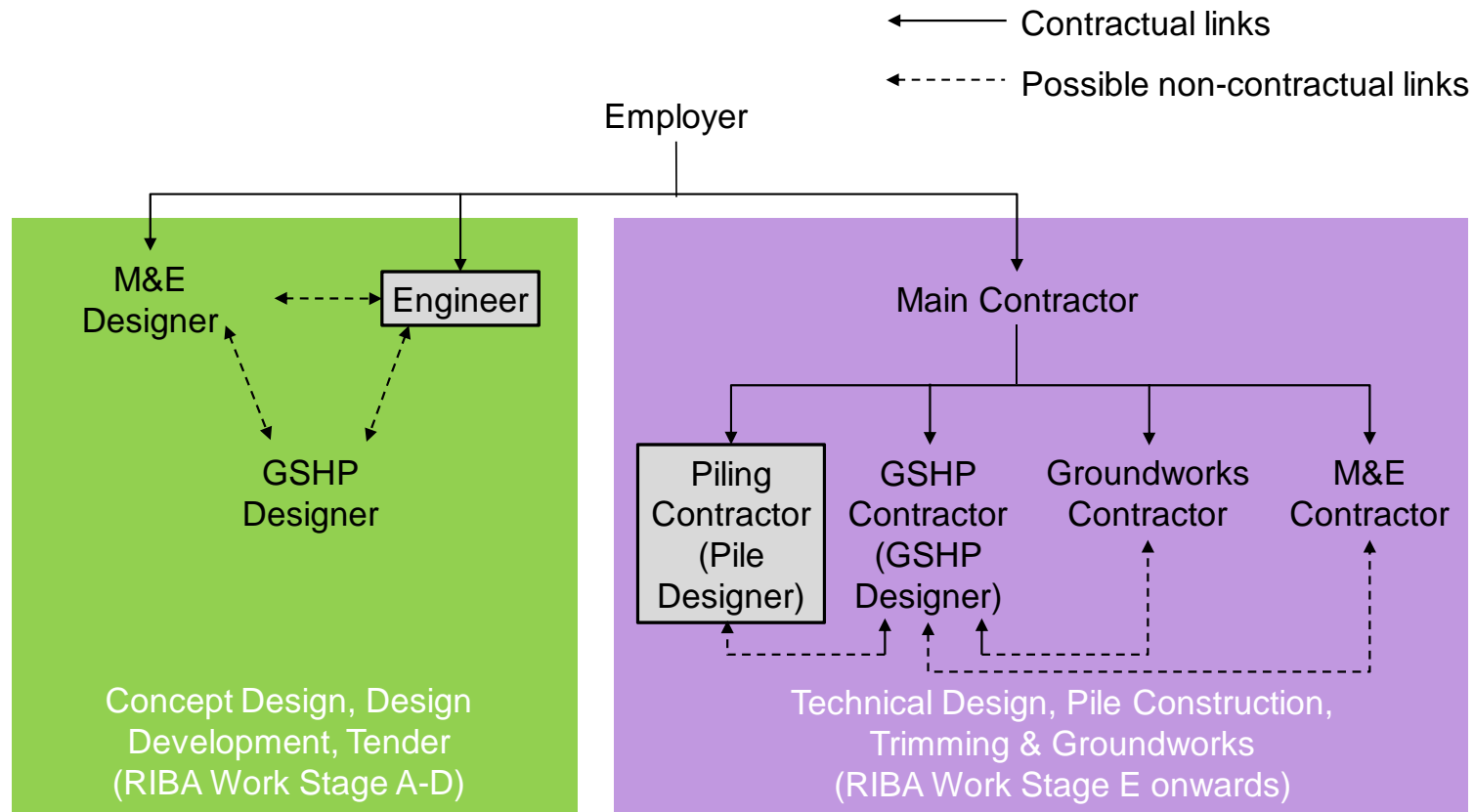
- “Engineer” design piles



Denotes parties with responsibilities set out in SPERW (2007)

Contractual responsibilities

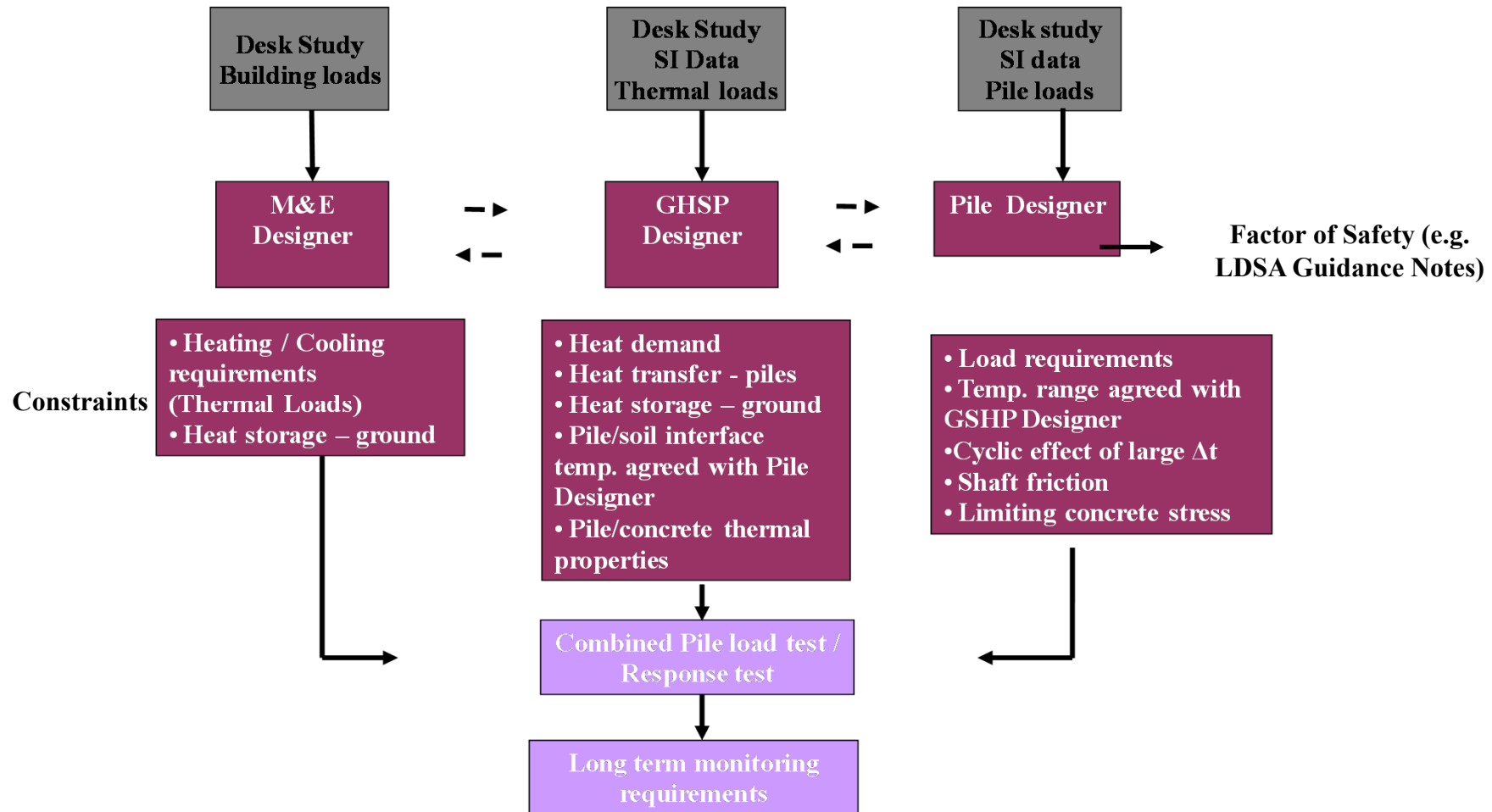
- **“Contractor” design piles**



Denotes parties with responsibilities set out in SPERW (2007)

Section 5 Design requirements

- Thermal effects complicate traditional pile design



Section 5 Geotechnical Pile design – heating pile

Building Load – effect on pile F of S?

Pile expansion/ contraction

ΔH

$\Delta T = 30^\circ C$

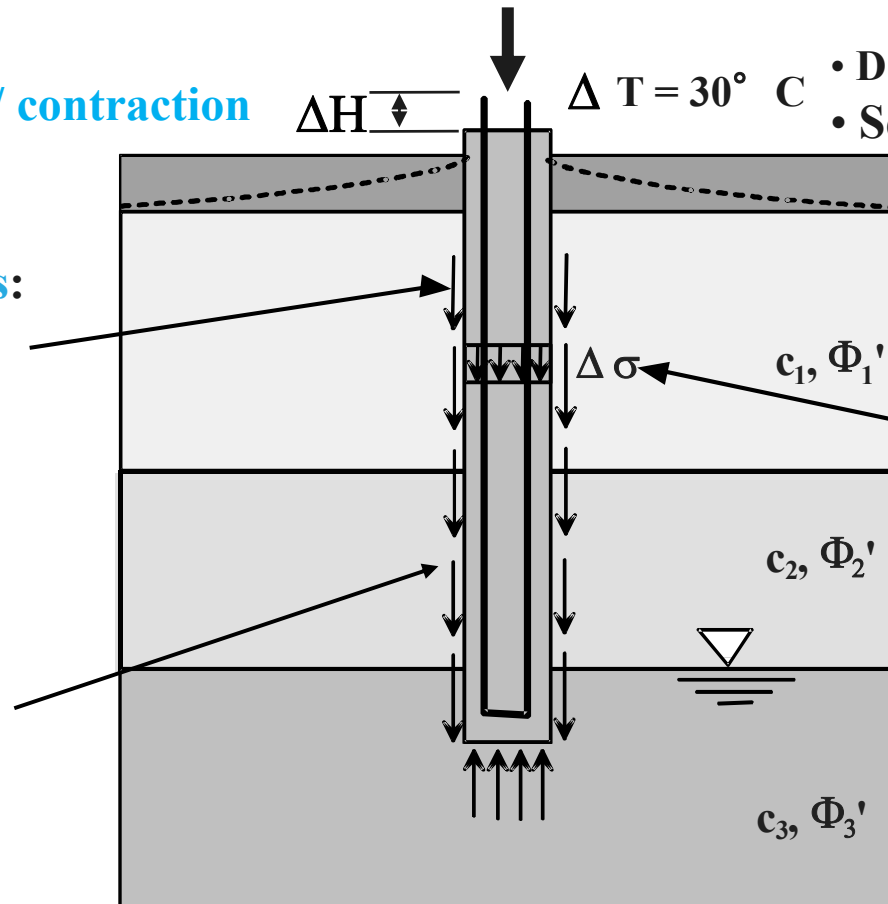
- Daily fluctuations
- Seasonal fluctuations

Shaft friction effects:

- Freezing?
- Shear stress?
- Radial stresses?
- Cyclic loads?
- W/C change?

Thermal Properties:

- Soils
- Concrete



Ground uplift?

Concrete Stress

- Stress concentrations next to pipes?

Geothermal Pile – Geotechnical Design Process

1. Pile design for structural loads

- Normal F of S > 2.0 to 3.0 – (ULS Design)
- Consider normally consolidated clays as –ve skin friction.

2. Agree temperature range with GSHP Designer

- Interface must not freeze. - Pile/Soil interface eg +2 to +30°C.
- Number of thermal piles – free head / Fixed head

3. Assess pile expansion and ground movements (Undrained)

- Free head and fixed head (SLS design)

4. Assess concrete stresses – dead load and thermal

- Max concrete stress < Concrete strength (q_c)/4

5. Consolidation / Quasi – thermal creep effect

- Check settlement

6. Check live loads and thermal cyclic effects

- Treat thermal loads as cyclic live loads - 50 annual cycles

Combined load and thermal test - Lambeth College, London (2007)

Bourne-Webb et al, (2009) Geotechnique

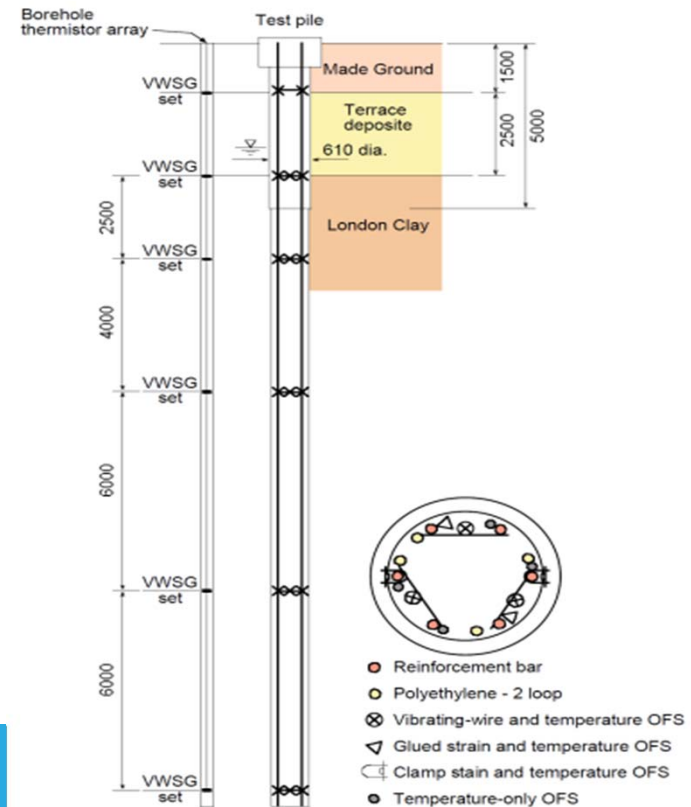
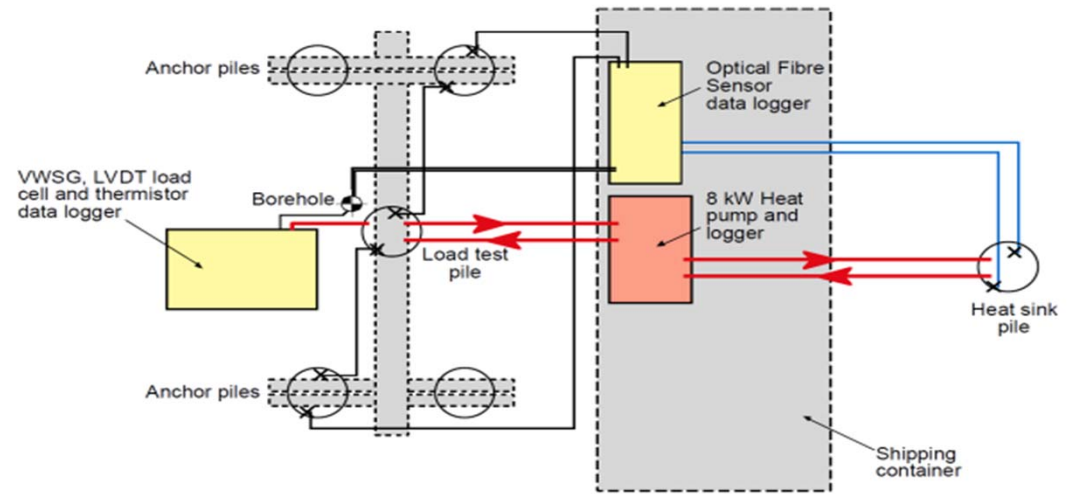
- **Cementation / GIL / Cambridge**
- **Pile loading test undertaken incorporating cyclic temperature effects**
- **Optical fibre sensor (OFS) system**
- **Conventional vibrating-wire strain gauges (VWSG), thermistors and external load control elements**

Lambeth College - Geotechnical Assessments

- **Rapid (Undrained) response –**
 - Expansion of pile - Lambeth College
- **Long term (Drained) response –**
 - Dissipation of pore pressure
- **Quasi Creep effect**
 - Reduction in Preconsolidation pressure with increased temp.
- **Cyclic thermal loading**
 - Annual thermal cycle

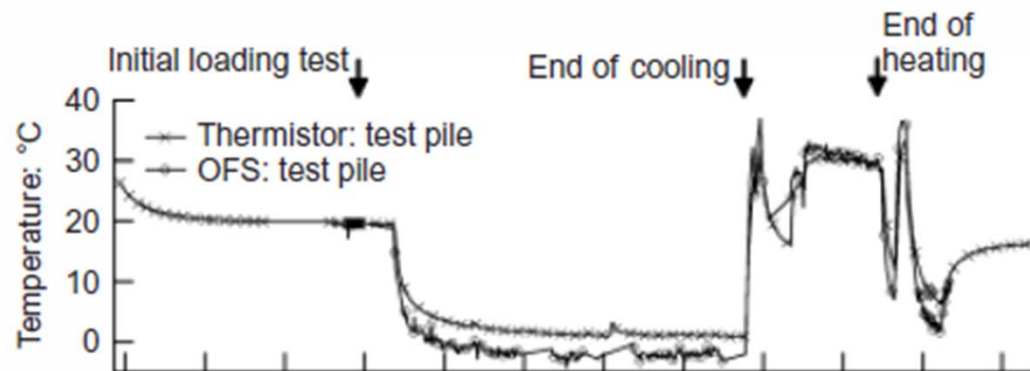
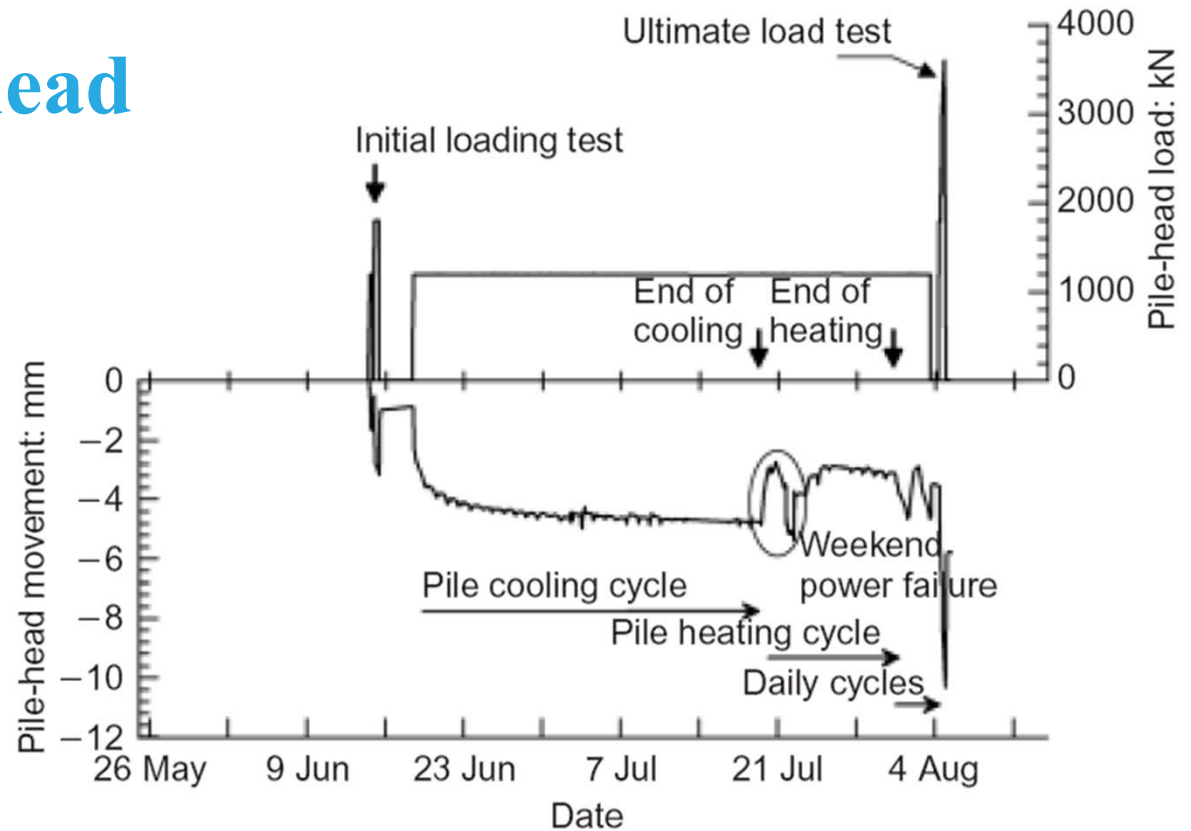
Lambeth College Pile Test

Layout and Instrumentation



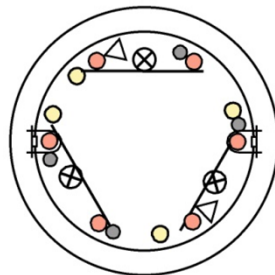
Pile Temp and head movement

- Design load -1mm settlement
- Cooling – 3mm change
- Heating – 2mm change
- Little heave during heating

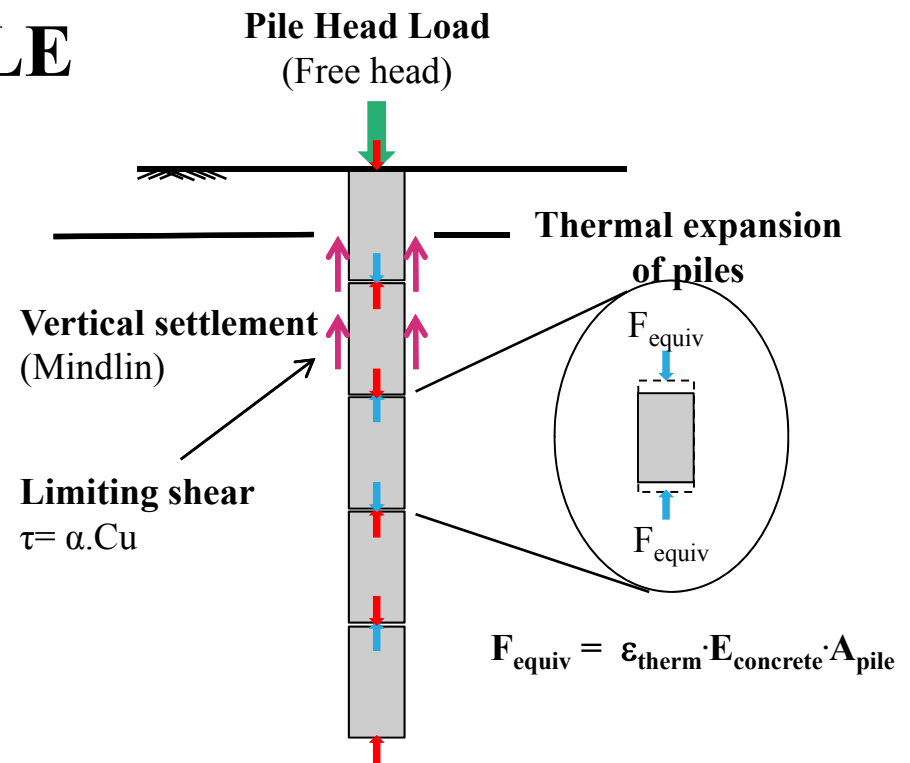


Lambeth College Modelling using DYNA and OASYS PILE

- Both external load and heating/cooling cycle applied to pile
- LS-DYNA and Oasys PILE used to model behaviour

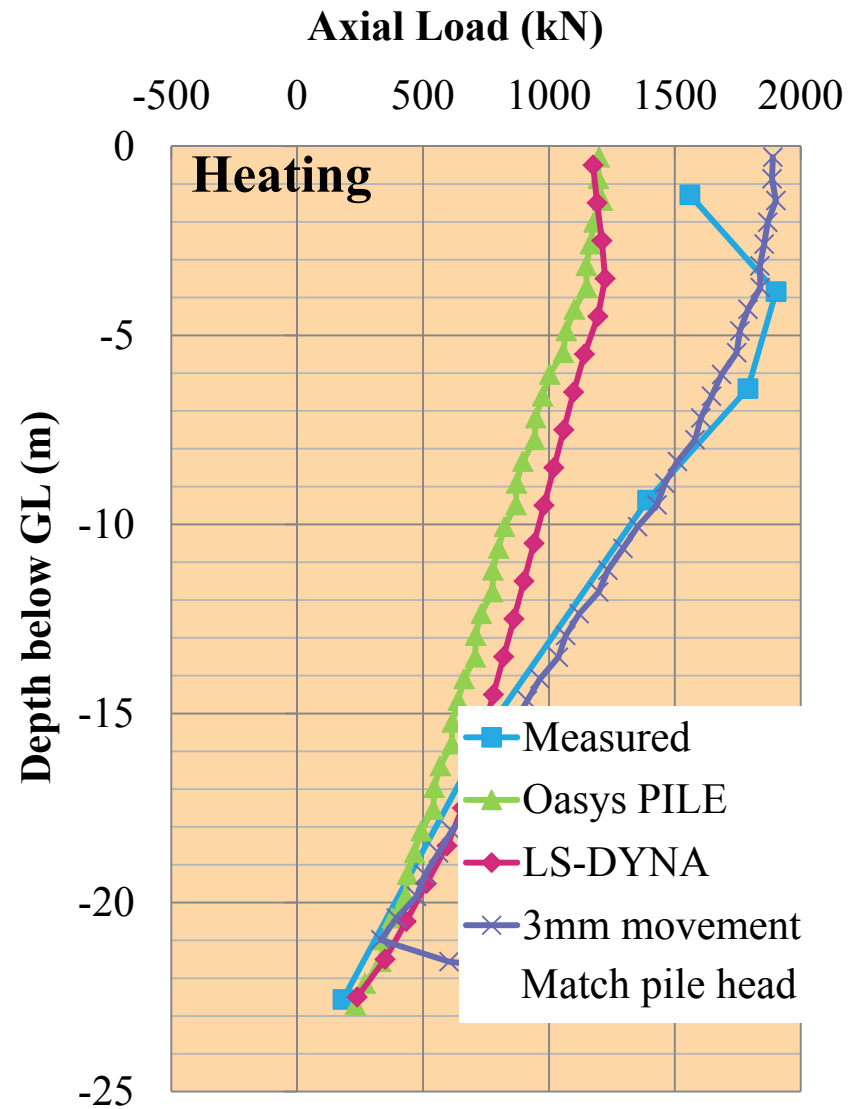
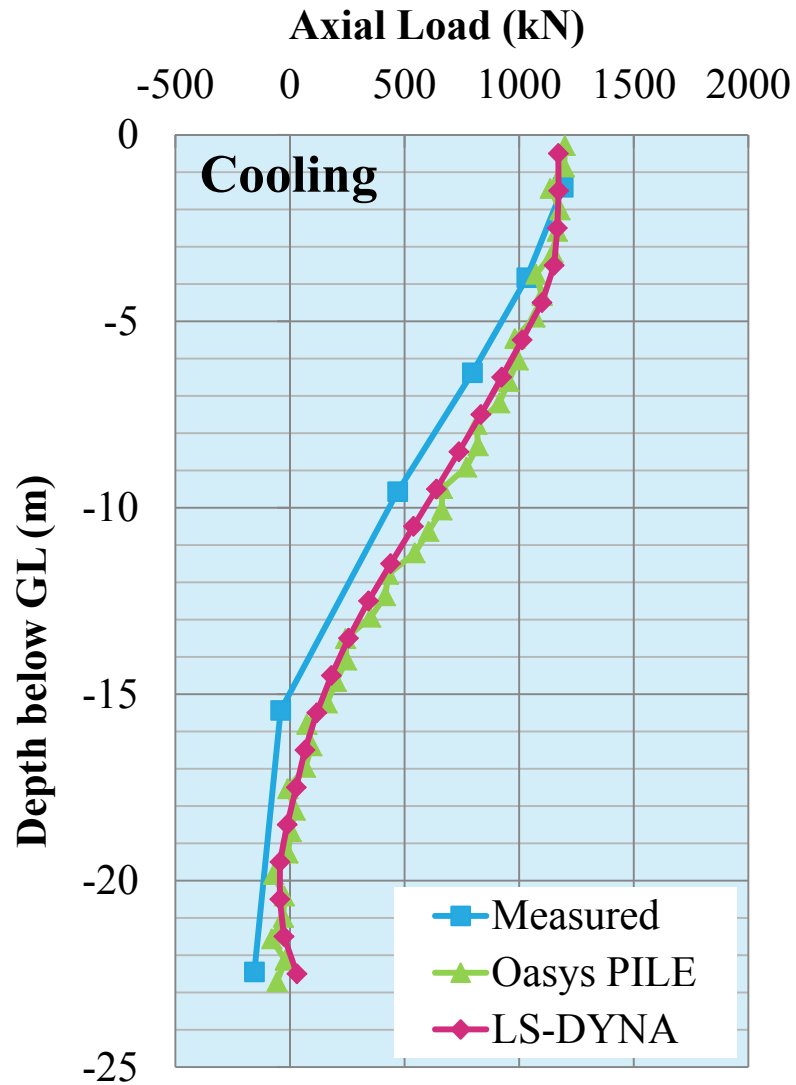


- Reinforcement bar
- Polyethylene
- ⊗ Vibrating-wire and temperature OFS
- ▽ Glued strain and temperature OFS
- ⊔ Clamp stain and temperature OFS
- Temperature-only OFS



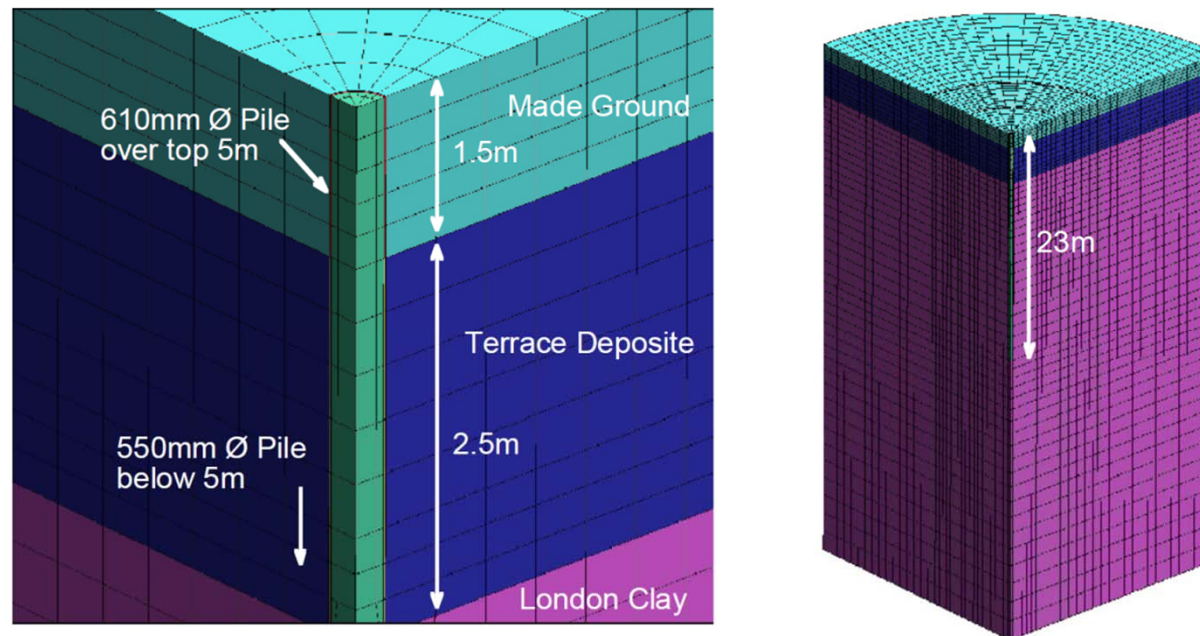
Lambeth College – Pile Loads

Fixed pile head generated large axial load



Lambeth College – Modelling pore pressures (In progress)

- **LS-Dyna calculates excess pore pressures due to:-**
 - Undrained pile loading 1200kN
 - Thermal effects
- **Dissipation of water pressures allows consolidation**



Section 5 - GSHP Design of thermal piles

- **Fleur Loveridge has addressed issues**
- **Pile Modelling Assumes**
 - line source – piles up to 0.3m – Use standard packages
 - Uniform temperature source – larger piles – Use Pile Sim or Orphius
 - Finite element models
- **Number of loops in pile**
- **Low thermal conductivity concrete – similar to soil**
- **High thermal conductivity concrete – reduces thermal resistance**

Lab Testing – pore pressures

- **Difference in soil/porewater thermal expansion generates excess pore pressures on heating**
- **Discussed in literature:**
 - Campanella & Mitchell (1968)
 - Hueckel, Francois and Laloui (2009)

α_s = thermal expansion of mineral solids

α_w = thermal expansion of soil water

α_{st} = physico-chemical structural volume change

$$\Delta u = \frac{n \Delta T (\alpha_s - \alpha_w) + \alpha_{st} \Delta T}{m_v}$$

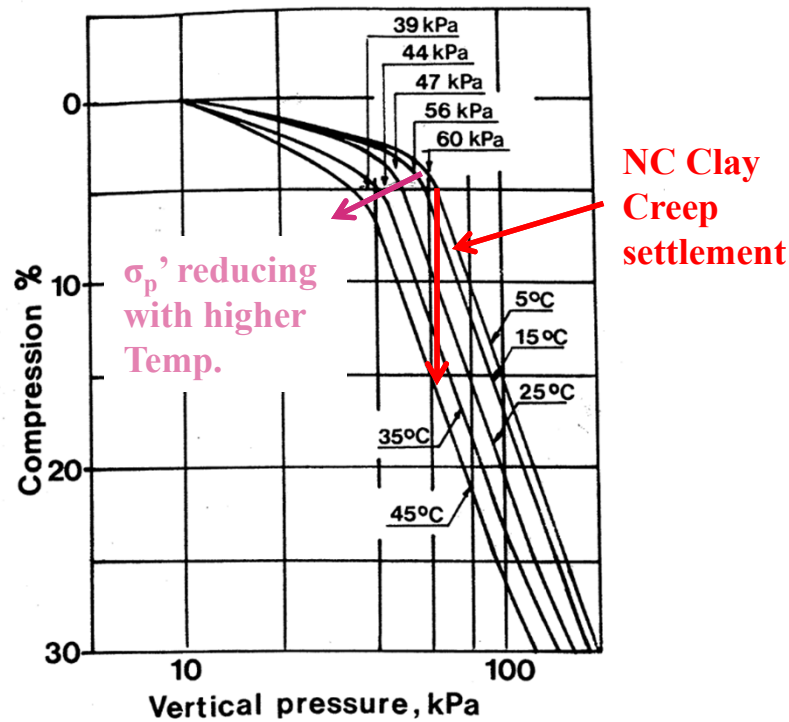
(Campanella & Mitchell, 1968)

m_v = soil compressibility

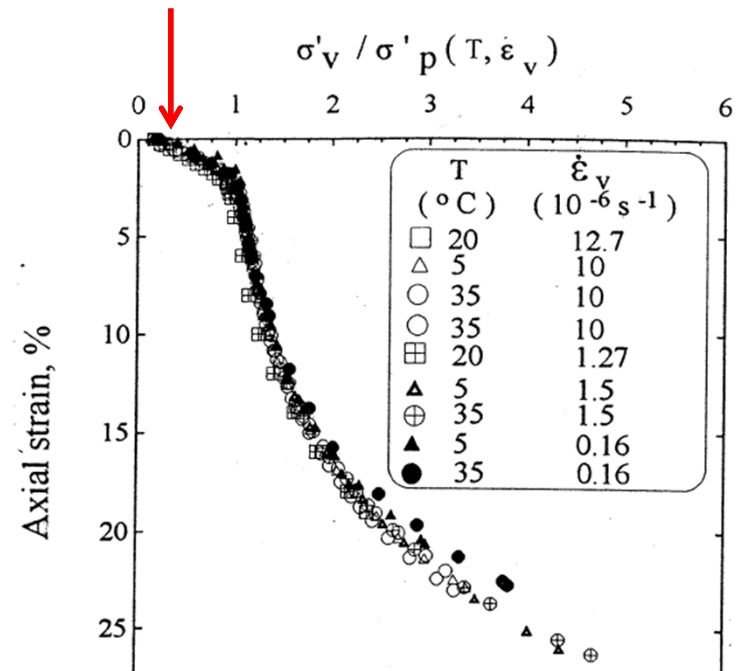
Thermal-creep effect on preconsolidation

- Heating reduces preconsolidation pressure (σ_p') and stiffness
- Creep ignored in OC clays NOT in NC clays.

London Clay is very over-consolidated.



(Eriksson, 1989)



(Boudali, Leroueil & Srinivasa Murthy, 1994)

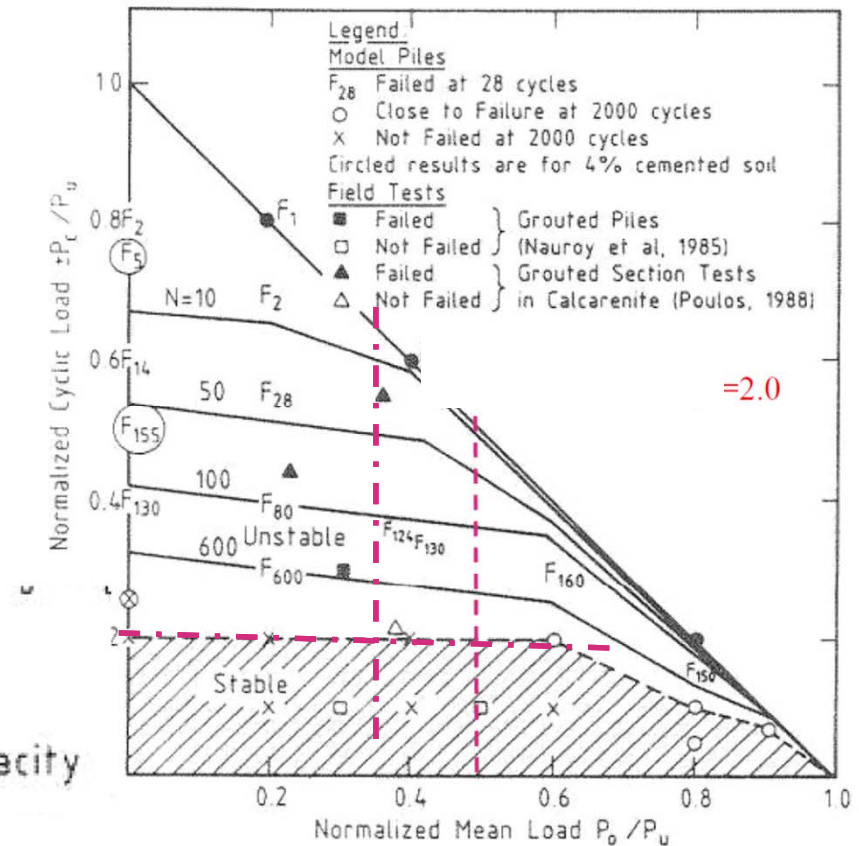
Cyclic loading

- **Cyclic thermal load caused by heating and cooling pile**

- $P_u = 3.6\text{MN}$
- $P_o = 1.2\text{MN}$
- $P_c = 0.7\text{MN}$

- $P_c/P_u = 0.7/3.6 = 0.2$
- $P_o/P_u = 1.2/3.6 = 0.33$

P_c = Cyclic load
 P_o = Mean load
 P_u = Static load capacity



Poulos Stability Diagram

Section 6 – Response Tests for thermal piles

- **How Long should the test take?**
- **Consider Loops on Centreline or round perimeter**
- **Thermal conductivity of concrete relative to soil**
- **Temperature at soil concrete interface**
- **Response test – shallow depth**
 - Part of Geotechnical Investigation
 - Part of pile test eg reaction pile
- **Combine with strain gauges mid depth – thermal stress in piles**

Section 7 Pipe Materials

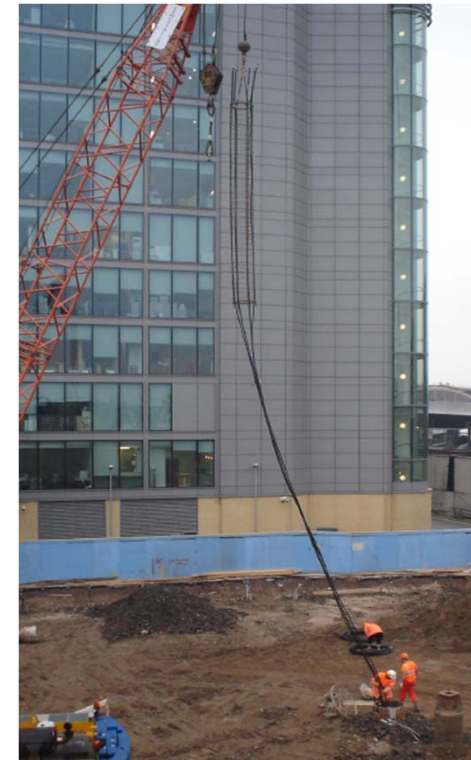
- **Plastic pipes - Bend Radius - PEX at 20°C**
 - 15/??mm -- ??m pile Can a 15mm PEX pipe fit in a 0.45m pile?
 - 20/1.9 mm - 0.6m pile (20cm)
 - 25/2.3mm - 0.75m pile. (25cm)
 - 32/2.9mm - 0.90m pile (32cm)
 - 40/3.7mm - 1.0m pile cage (40cm)
- **PE100 or PE100+ at 20°C**
 - 15/??mm -- ??m pile
 - 20/1.9 mm – 1.0m pile (40cm)
 - 25/2.3mm - 1.2m pile. (50cm)
 - 32/2.9mm - 2.2m pile (100cm)
 - 40/3.7mm - N/A
 - PEX bends to about half the radius of PE100 or PE100+.
 - Colder temperatures increase min bend radius
 - PEX is more expensive but does not need U bends at the top and bottom of loops.

Section 10 Loop Installation

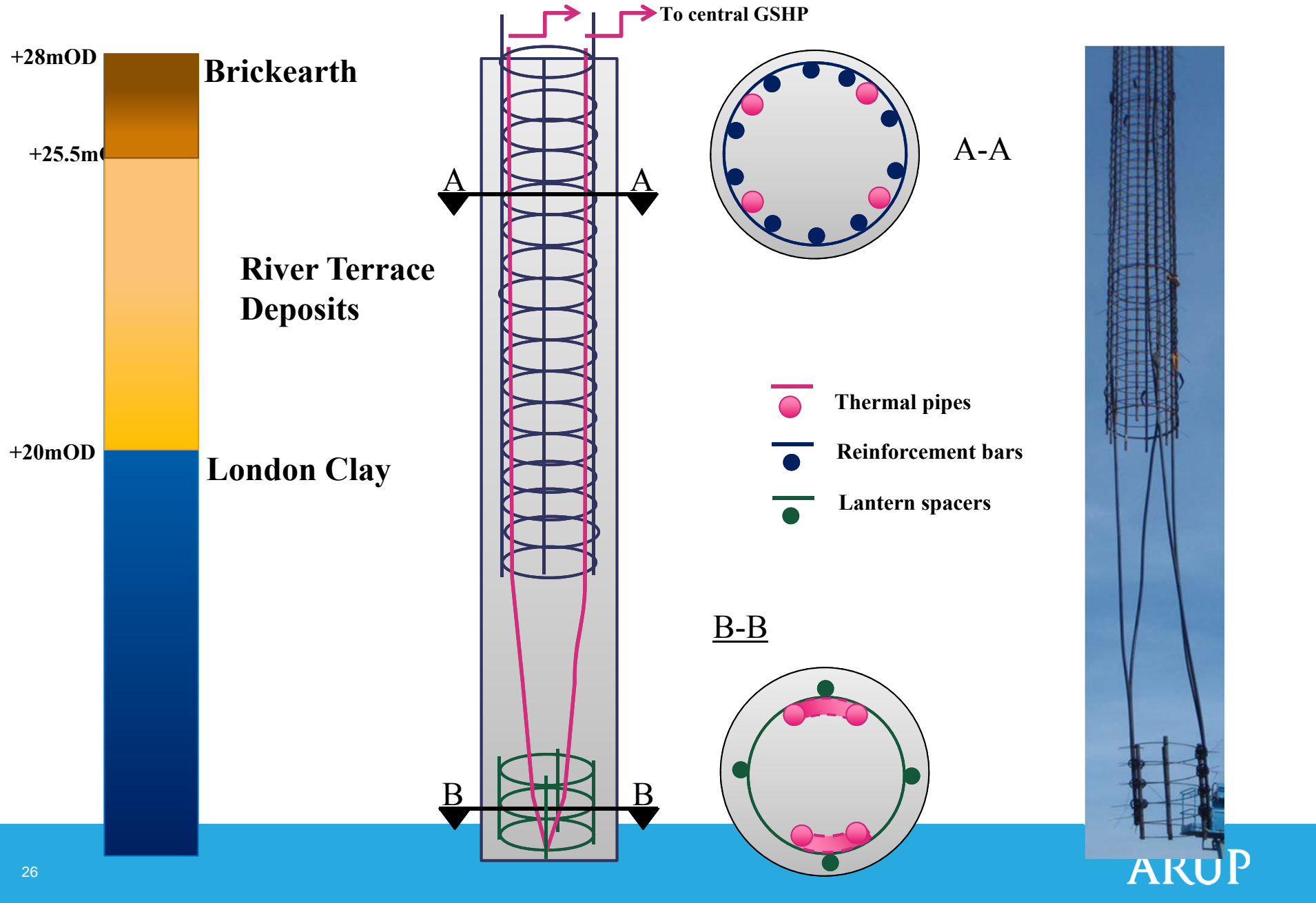
- **Loops on long cages – Long tremie pipe**
 - Inside cage
 - Outside cage
- **Loops on short cages – Short Tremie**
 -

Section 10 Borehole Loops installation

- **Historically – Europe**
 - Long cages
 - Internal pipes with looped pipes
- **In London - dry bored piles**
 - Use short cages
 - Use borehole U-tubes
- **Paddington Basin – GIL and Cementation**
 - Two pairs of U-tubes

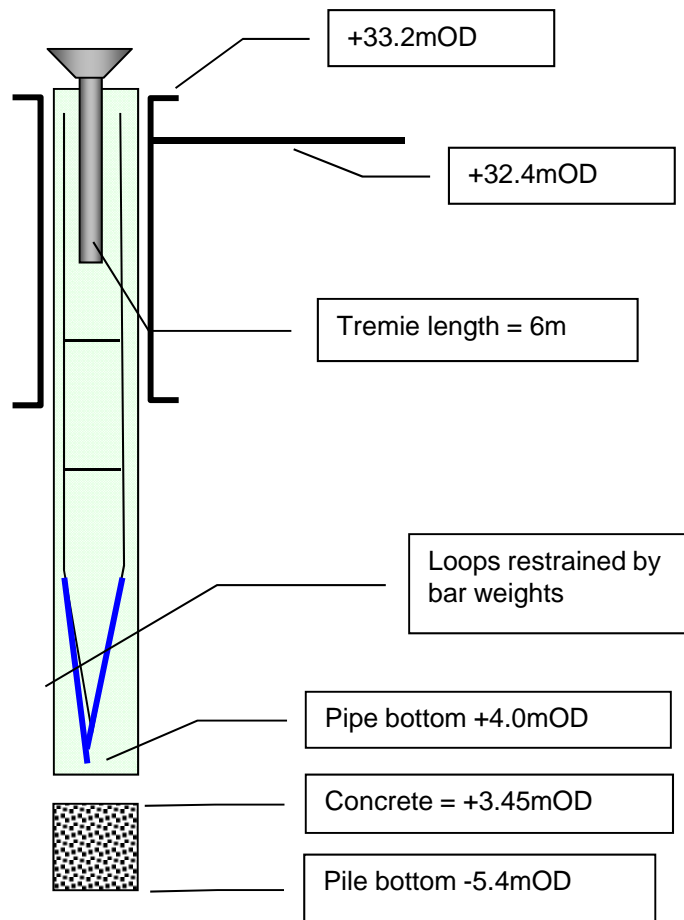


West End Green – Use of lantern spacers (2010)



Short or long tremie – Scratching test (2010)

Test set-up



Photos from test



Bar weights prior to testing



U bend after test



Upper pipe after test

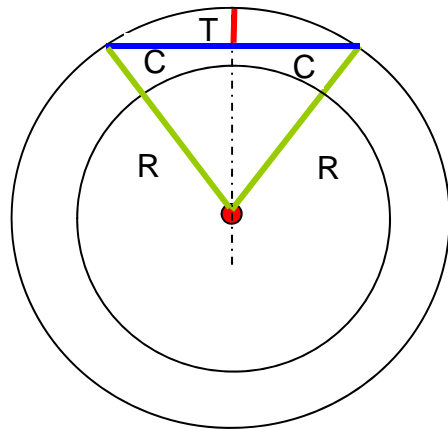


Lower pipe after test

Scratch depth measurement on 32mm pipes

■ Assessment of damage

- Par off pipe until scratch just disappears
- Measure pared width ($2C$)
- Calculate scratch depth



2C – chord length (mm) - measured;
T – Depth of the scratch (mm) - calculated
R – radius of the pipe – measured

Conclusions

- Vertical pipes – <1mm scratches
- Splayed pipes - 1 to 2mm scratches



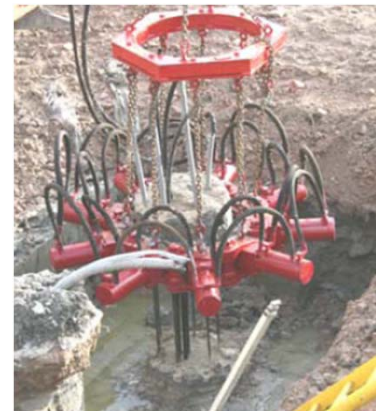
CFA Piles, Cambridge (Bachy Web site)

- **Pile design - Motts**
- **Pile Contractor – Bachy**
- **Loop design / build – GIL**
- **CFA piles (600mm dia)
150 No up to 25m depth**
- **Loops - 4 pipes x 32mm dia**
- **Pushed with 1 x T32**

- **Heating - 188kW**
- **Cooling - 117kW**



Plunging used T32 bar + 4 pipes (2 loops)



Trimming



Cage and header pipes

Section 11 Pressure testing

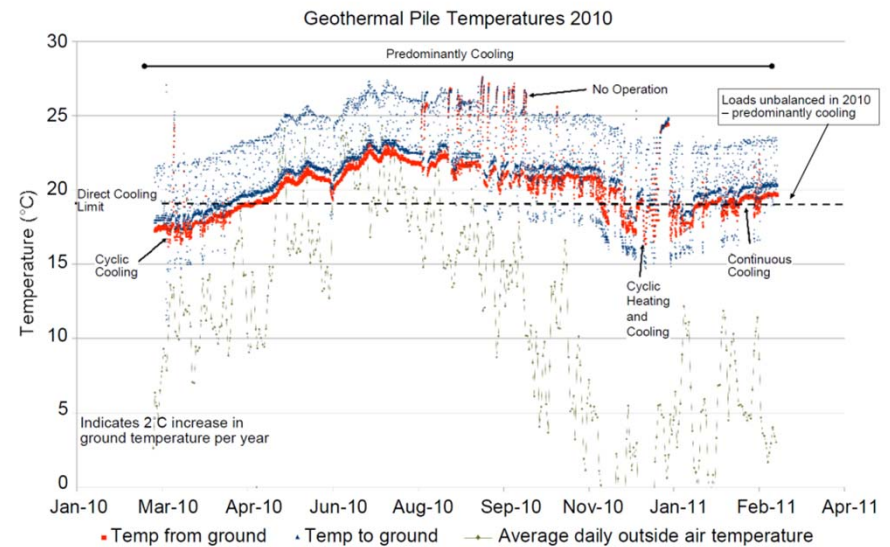
- **Checks for loop leakage**
 - During installation
 - Contract interfaces
- **Pressurise loops during installation**
 - European contractors pressurise loops during installation
 - UK does not do this?
- **Relevance of pressure test in concrete**
 - Pipe relaxation at high pressures
 - Stiff response increases test sensitivity
 - Pipe pressure can increase – Pile concrete heats water - expansion

Section 15 Monitoring and triggers

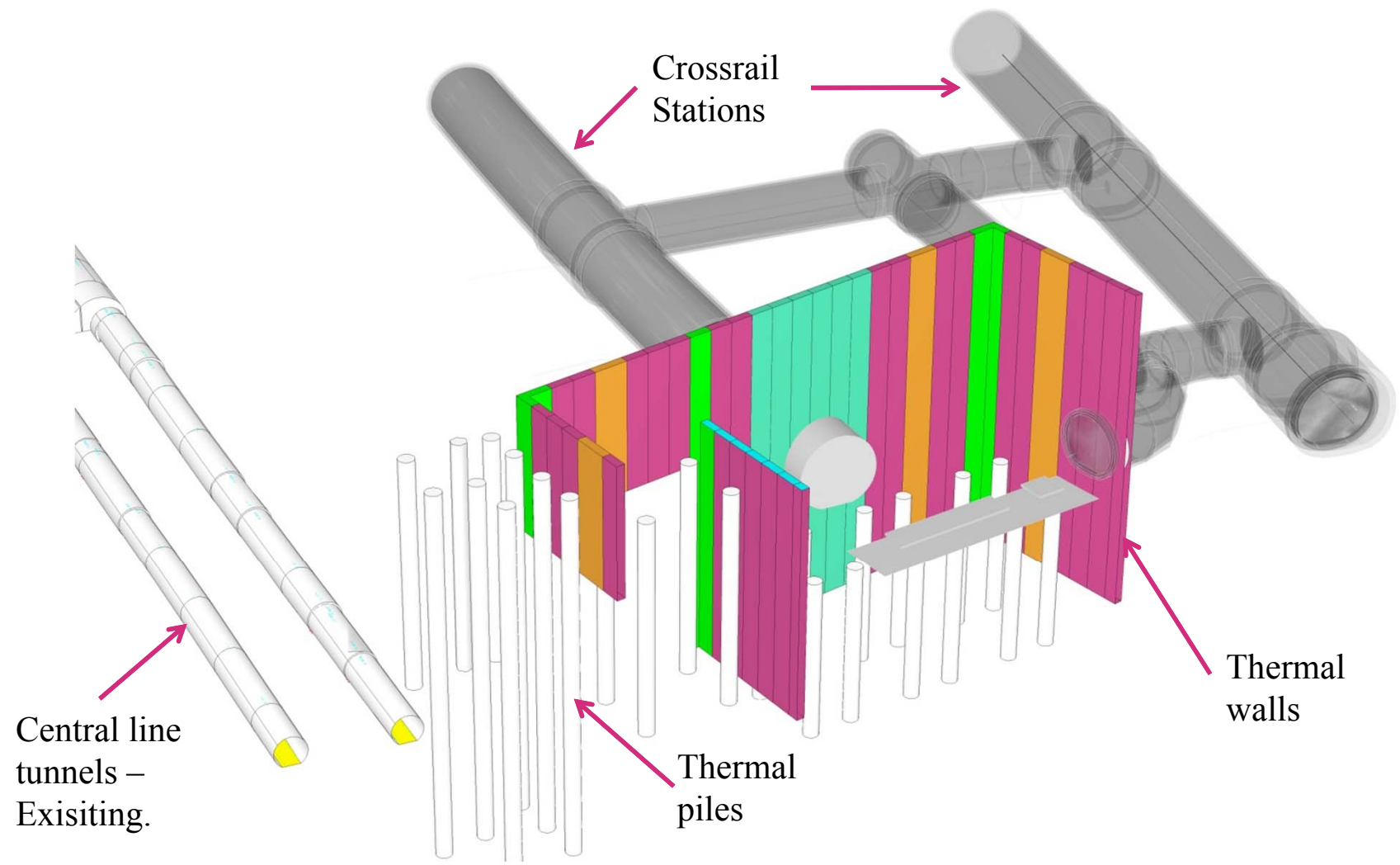
- No freezing at Soil/Pile interface
- Little data on relationship between circulation fluid temp and interface temperature
- Adopt conservative minimum temperature from heat pump
- Monitor
- Use trigger values
- Under discussion



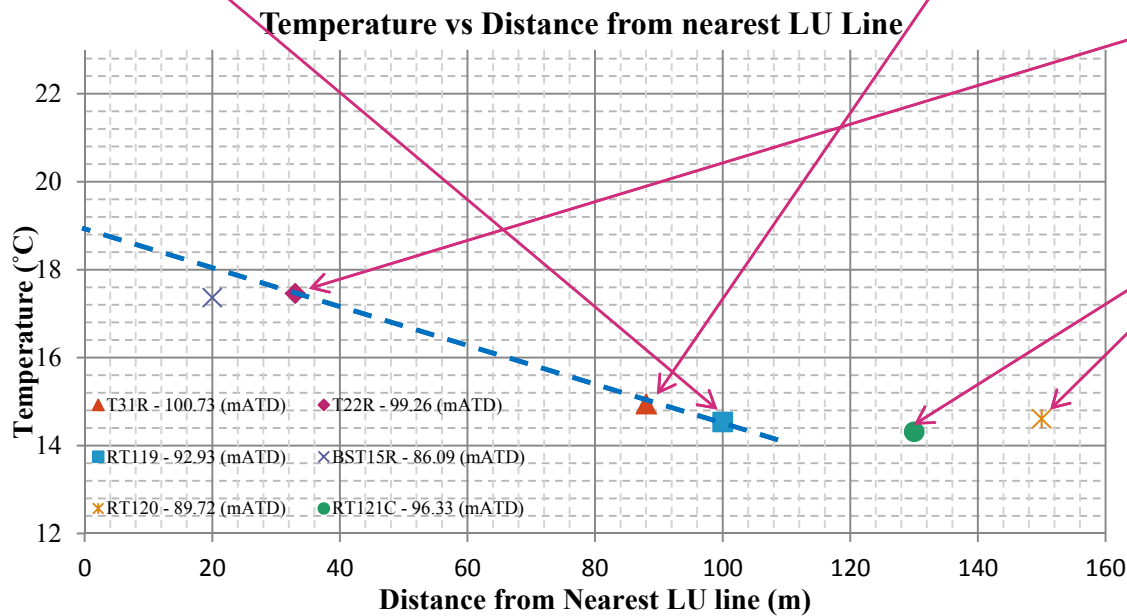
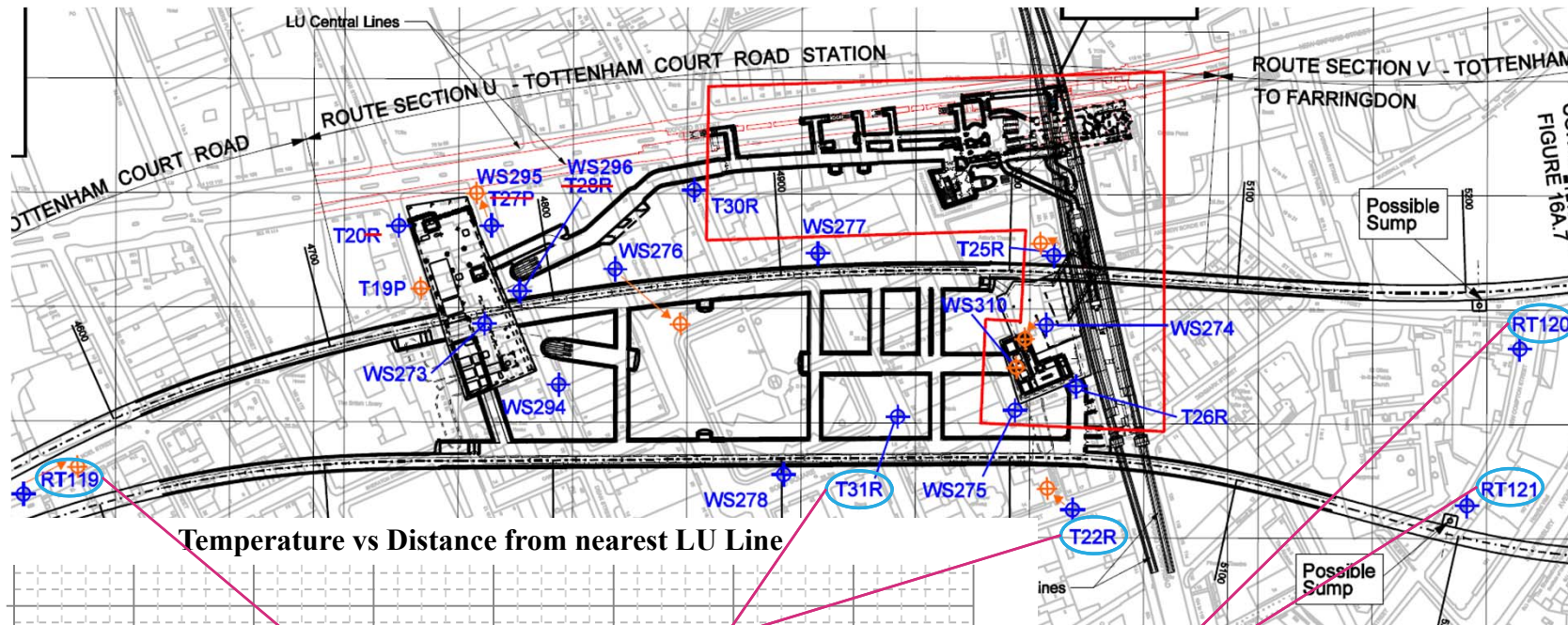
Keble College - Oxford



Thermal Walls – Crossrail Dean Street Box



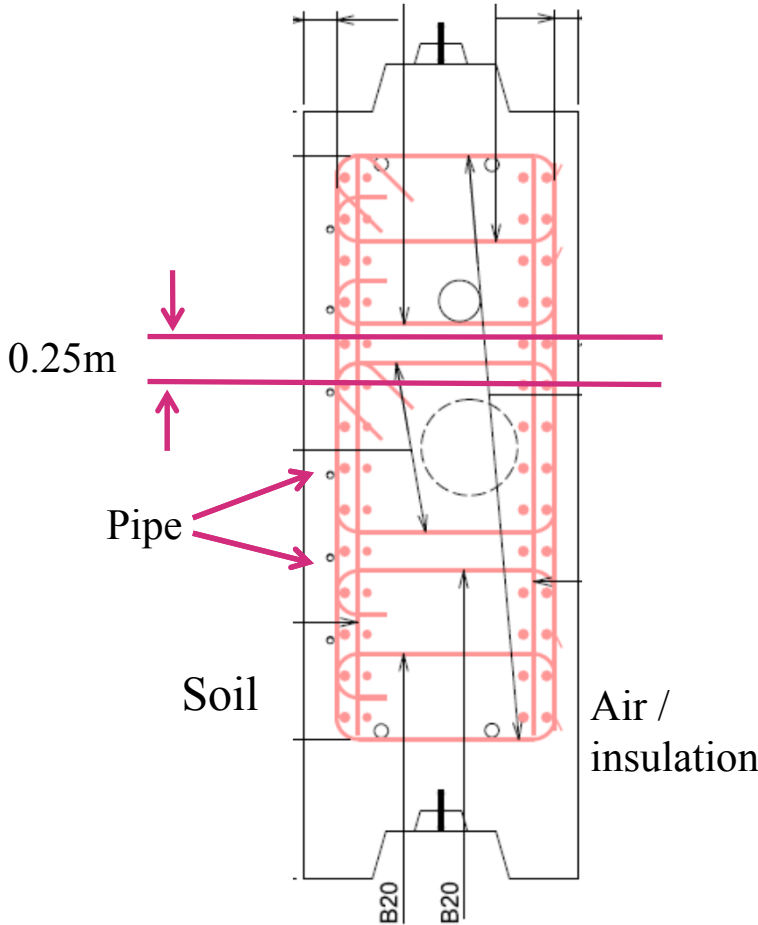
Crossrail - Ground temperatures at Oxford Street



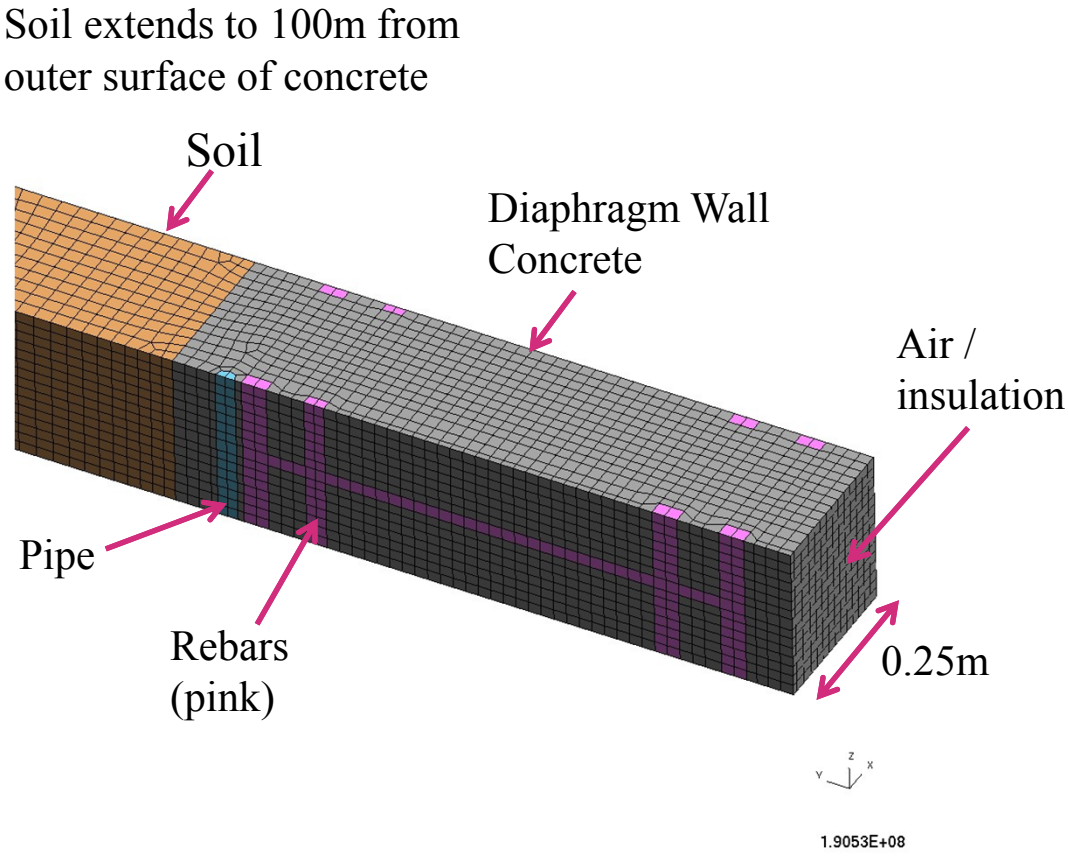
- Ground temperature at tunnel level
- Next to tunnel temperature 19°C
- Temperature drops to to ~15°C at about 90m from tunnel

Diaphragm wall

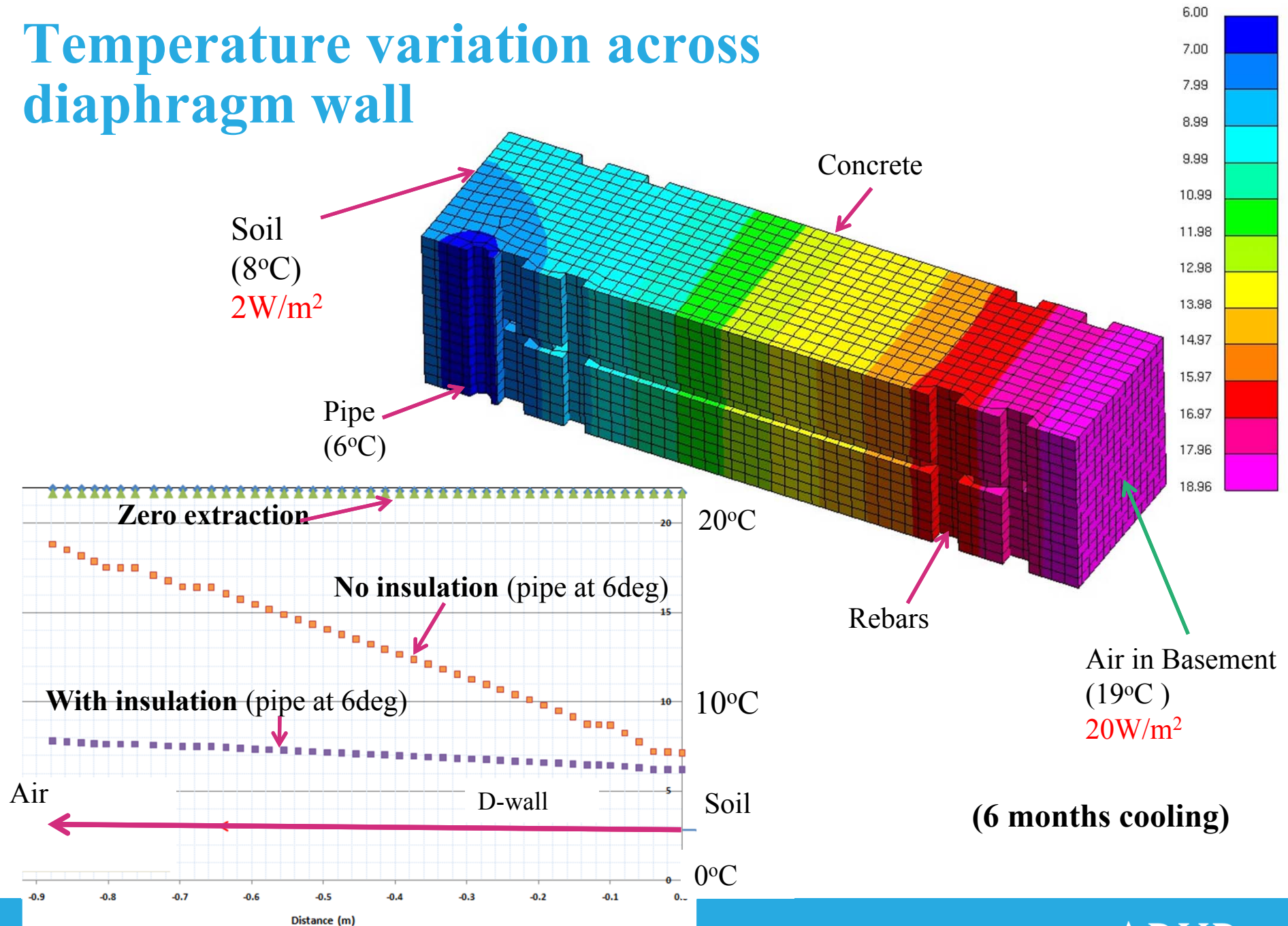
Dyna Model - Temperature effect on wall



PLAN VIEW

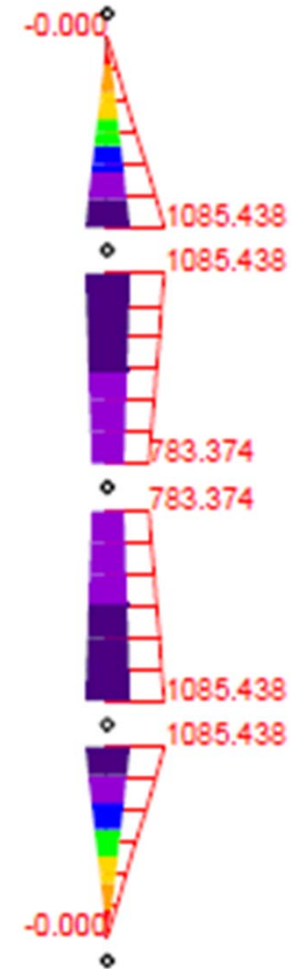
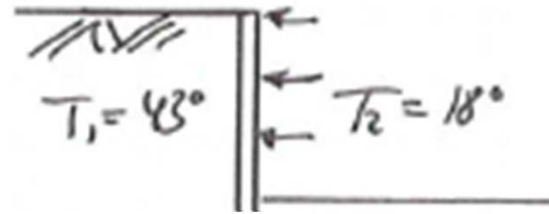
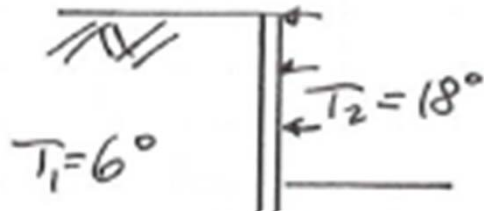


Temperature variation across diaphragm wall

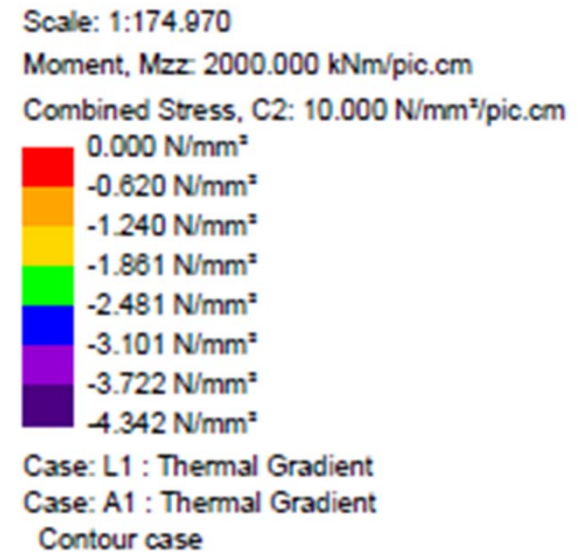


Thermal effects on wall bending moments

(Expansion of soil not considered)



(Cracked sections)



Conclusions -Thermal pile standard advances

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Thank you for your attention

- **Any Questions?**

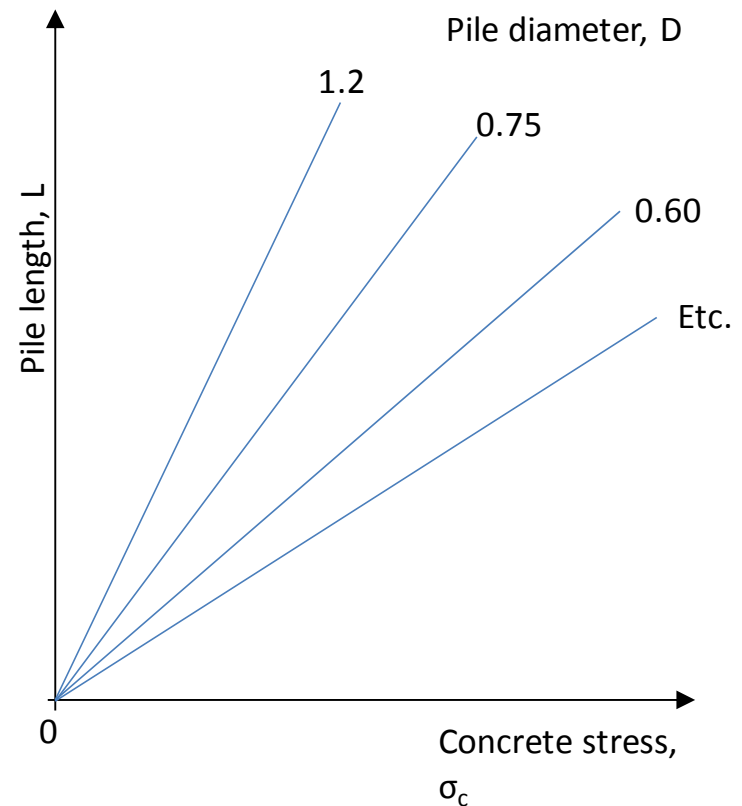
Thank you!

■ References

- Campanella, R.G. & Mitchell, J.K. (1968) Influence of temperature variations on soil behaviour, *Journal of the Soil Mechanics and Foundations Division*, 94(SM3), ASCE, pp 709-734.
- Boudali, M., Leroueil, S. & Srinivasa Murthy, B.R. (1994) Viscous behaviour of natural clays, *Proc. 13th Int. Conf. Soil Mechanics and Foundation Engineering*, New Delhi, pp 411-416.
- Eriksson, LG, (1989) Temperature effects on consolidation properties of sulphide clays, *Proc. 12th Int. Conf. Soil Mechanics and Foundation Engineering*, Rio de Janeiro, Vol. 3: pp 2087-2090

Design requirements – design charts

- **Design basis**
 - Thermal pile load test
 - Computer model
- **Typical temperature range to consider**
 - ± 5 to 10°C daily
 - $\pm 20^\circ\text{C}$ seasonal
- **Model of varying length/diameter of piles and study effect on concrete stress, FOS.**



Further work

- **Ongoing research provided in Appendices to the Thermal Pile Standard**
 - Soil and concrete thermal conductivity
 - Thermal response test interpretation for larger diameter piles
 - Change in soil behaviour / shaft friction / concrete stress with temperature variations
 - Pile / soil interface zone temperature and thermal conductivity
- **Knowns and unknowns in producing the design guidance clearly stated**
- **Several further revision cycles required to finalise the document with the T&SC**

Conclusions

- **Thermal Piles are established in UK.**
- **Thermal Pile / Heat pump systems - compete with gas boilers, biomass, CHP.**
- **Thermal pile installation methods developing.**
 - Need to check installation damage.
- **Geothermal design based on borehole loops guidance.**
- **Geotechnical design developing.**
- **Ownership of design responsibilities unclear.**
- **Few designers and contractors able to tender for work.**
- **Thermal walls – Design processes under development**
 - Basement insulation, thermal stresses on wall moments, earth pressures.

Design requirements – laboratory testing

- **Thermal conductivity - concrete**
 - Soil, concrete and interface zone
 - Eurocode or ASTM methods (eg Guarded hot plate)