

GSHPA Workshop
16 November 2011

**Soil-structure interactions for thermal
piles/walls; Fundamentals; Design
considerations; Future research needs**

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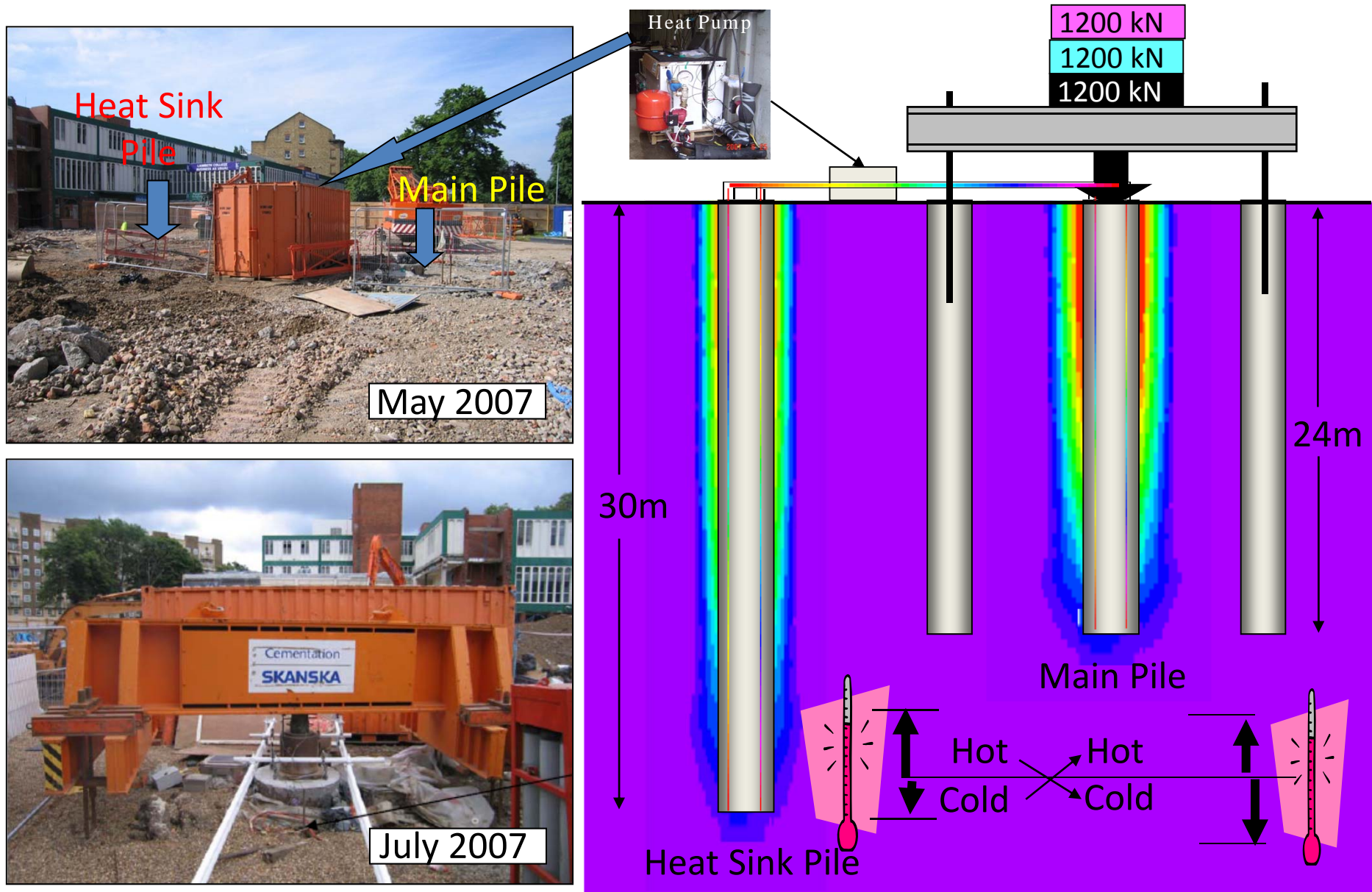
Acknowledgement

- Former and current researchers: Binod Amatya, Echo Ouyang, Ray Yi, Denis Garber, Yi Zhang, He Qi, Maria Canellas
- Peter Bourne-Webb
- Cementation Skanska – Peter Smith, Rab Fernie, Martin Pedley, Andrew Bell
- Geothermal International – Tony Amis, Chris Davidson
- Arup – Duncan Nicholson, Anton Pillai, Paul Bailie

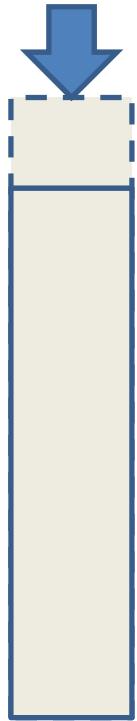
Current research projects at Cambridge

- Field study on long-term behaviour of thermal piles
- A pile-raft-structure interaction code for thermal piles
- Thermo-Hydro-Mechanical finite element code for thermal piles/tunnels/walls
- Interaction modelling of building performance and GSHP (boreholes, thermal piles/tunnels/walls)
- Capacity of GSHP systems at city-scale
- Thermal response testing

Mechanical Load Tests coupled with thermal loading



External Loading
– Building load



Greater stress –
more strains

Internal Loading – Thermal load

Free expansion
(soft base, pile groups)

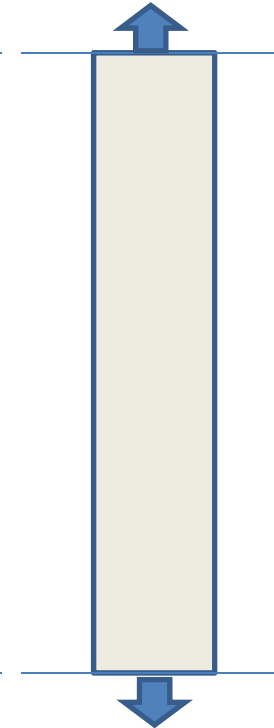
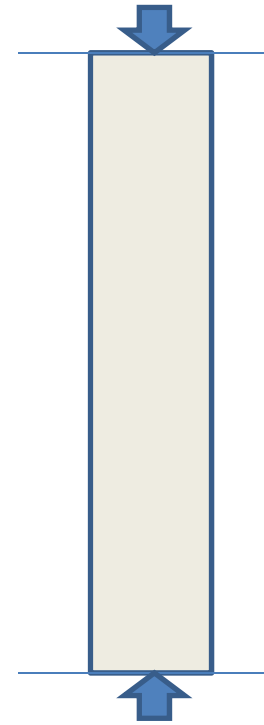
End constraints
(hard base, stiff structure)

Heating

Cooling

Heating

Cooling

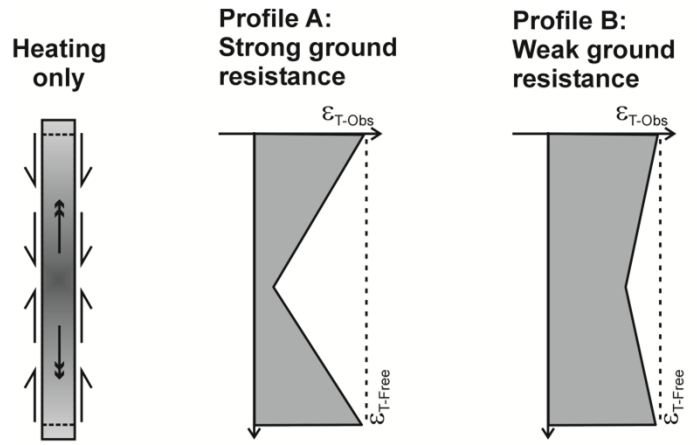


No stress

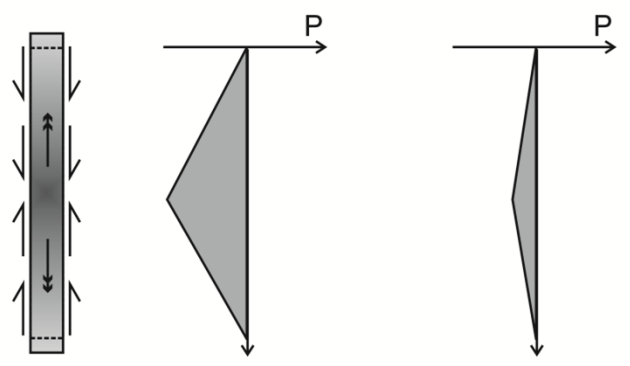
No strain

Expansion Shrinkage

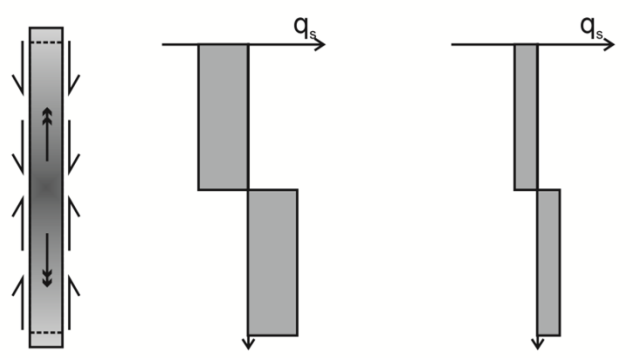
Compression Tension



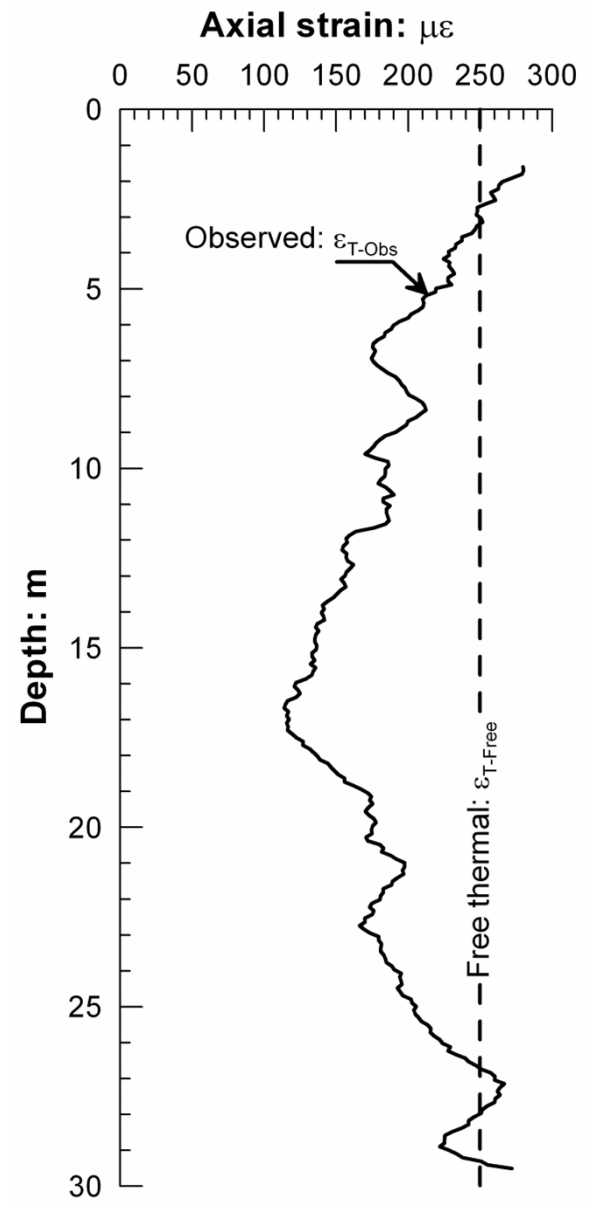
a) Axial thermal strain profiles



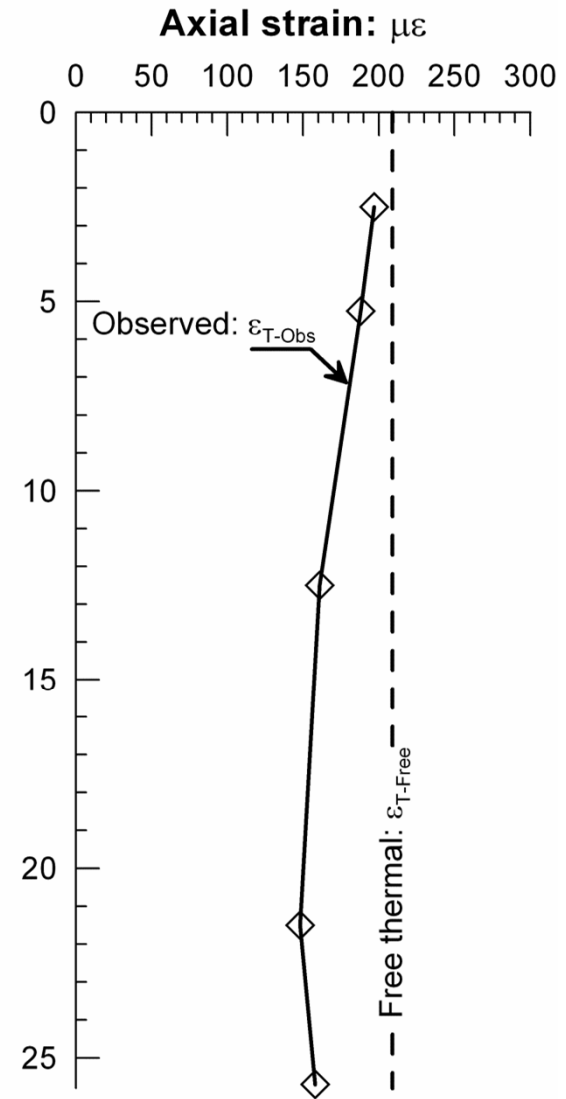
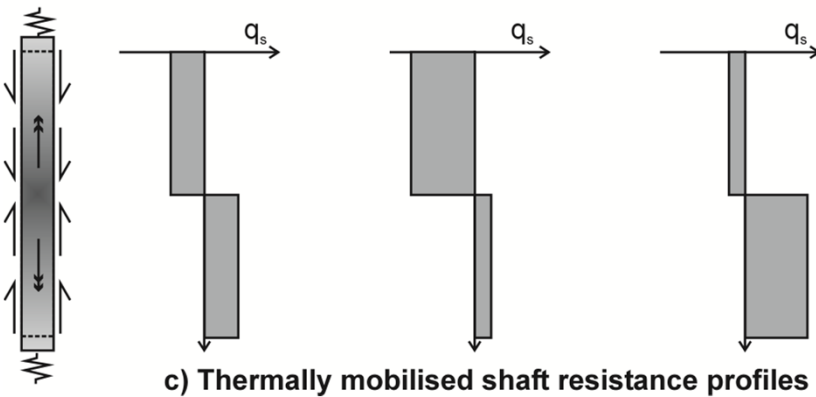
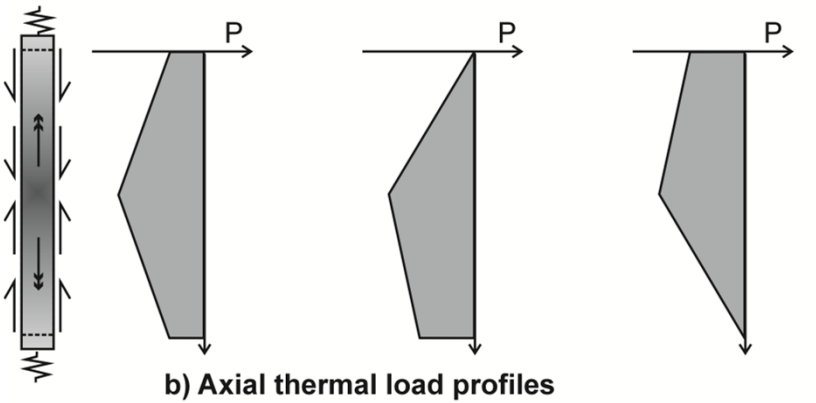
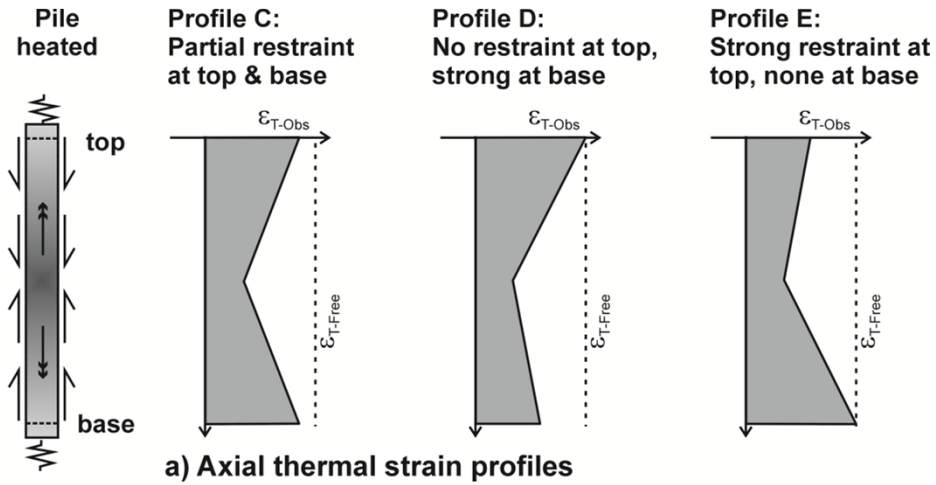
b) Axial thermal load profiles



c) Thermal mobilised shaft resistance profiles

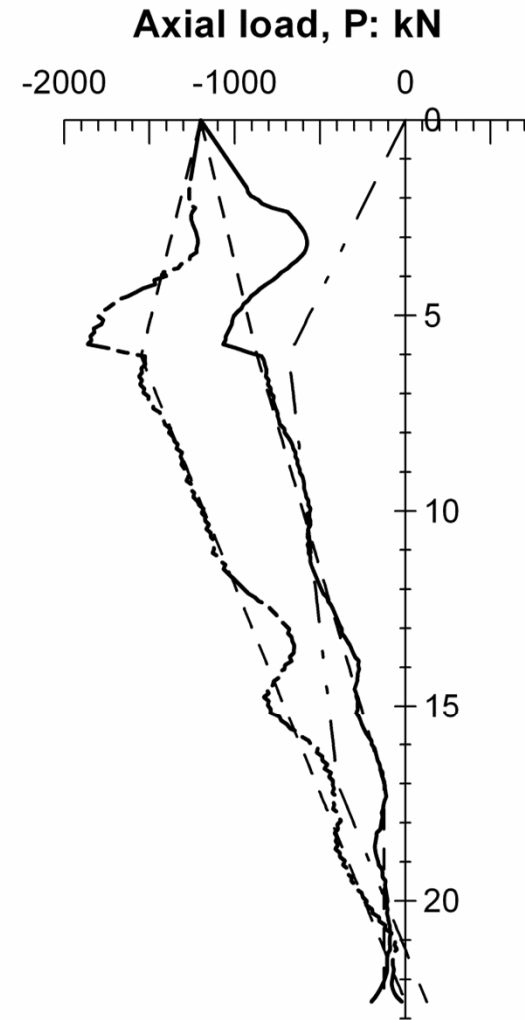
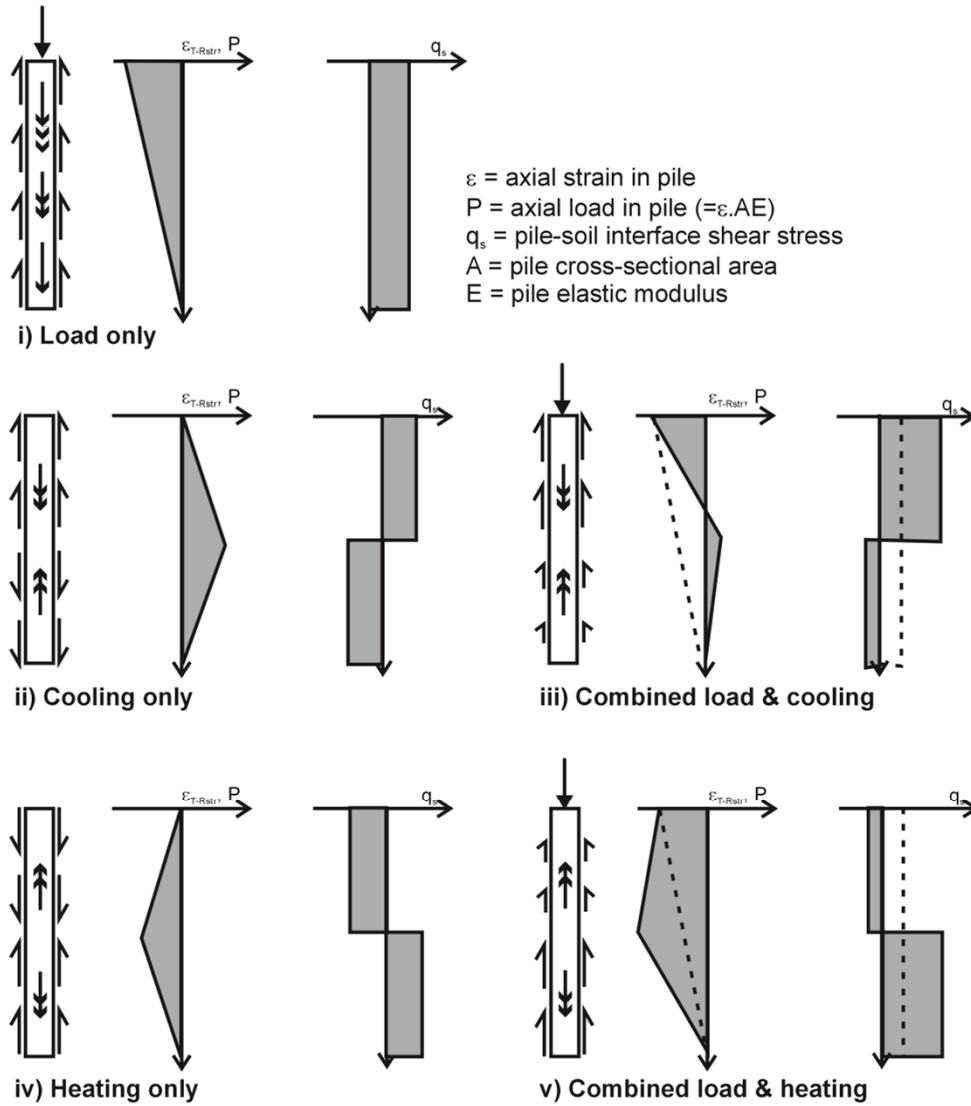


a) London Heat Sink pile:
 $\Delta T = 29.4^\circ\text{C}$



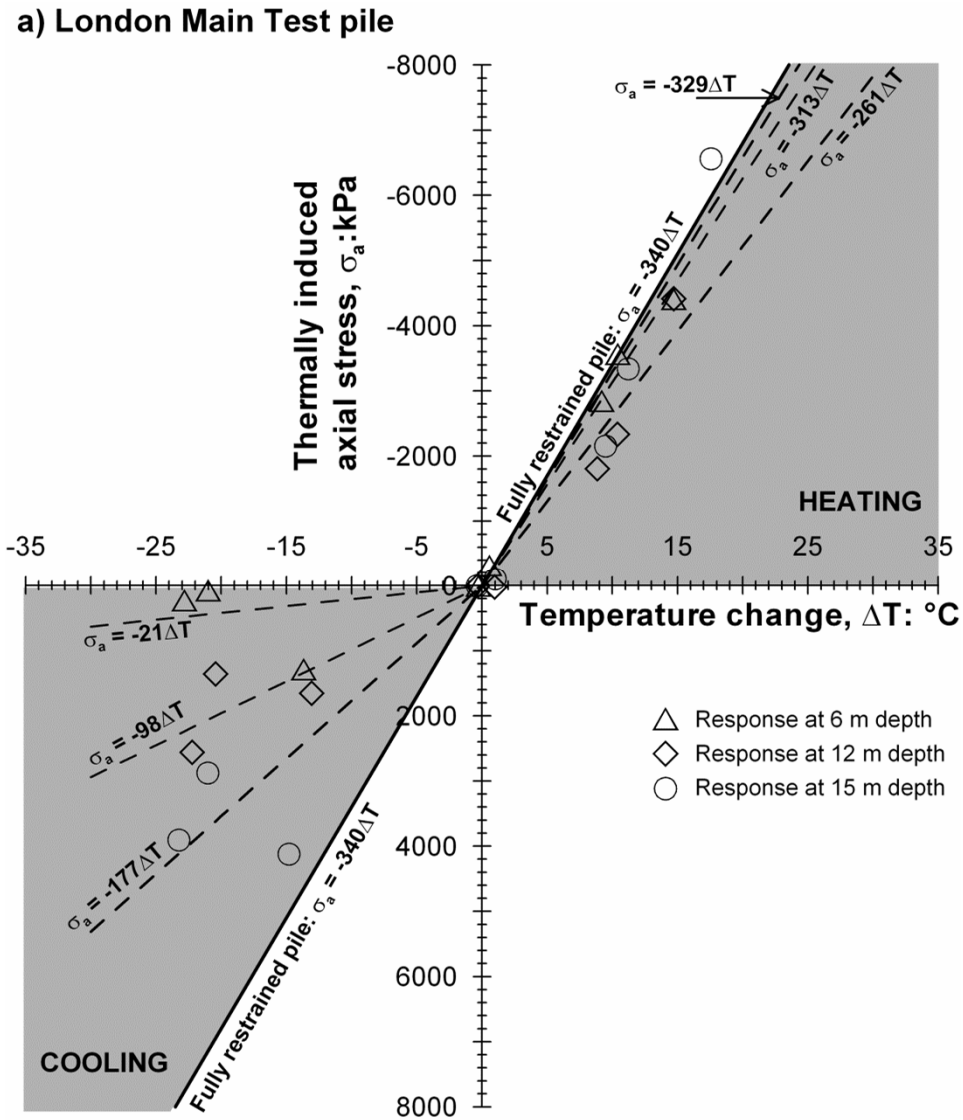
b) Lausanne T-1 test:
 $\Delta T = 20.9^\circ\text{C}$

a) Heating & cooling with no end restraint, after Bourne-Webb et al (2009, in print)



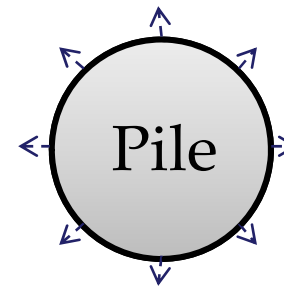
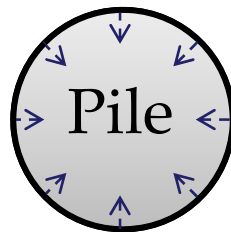
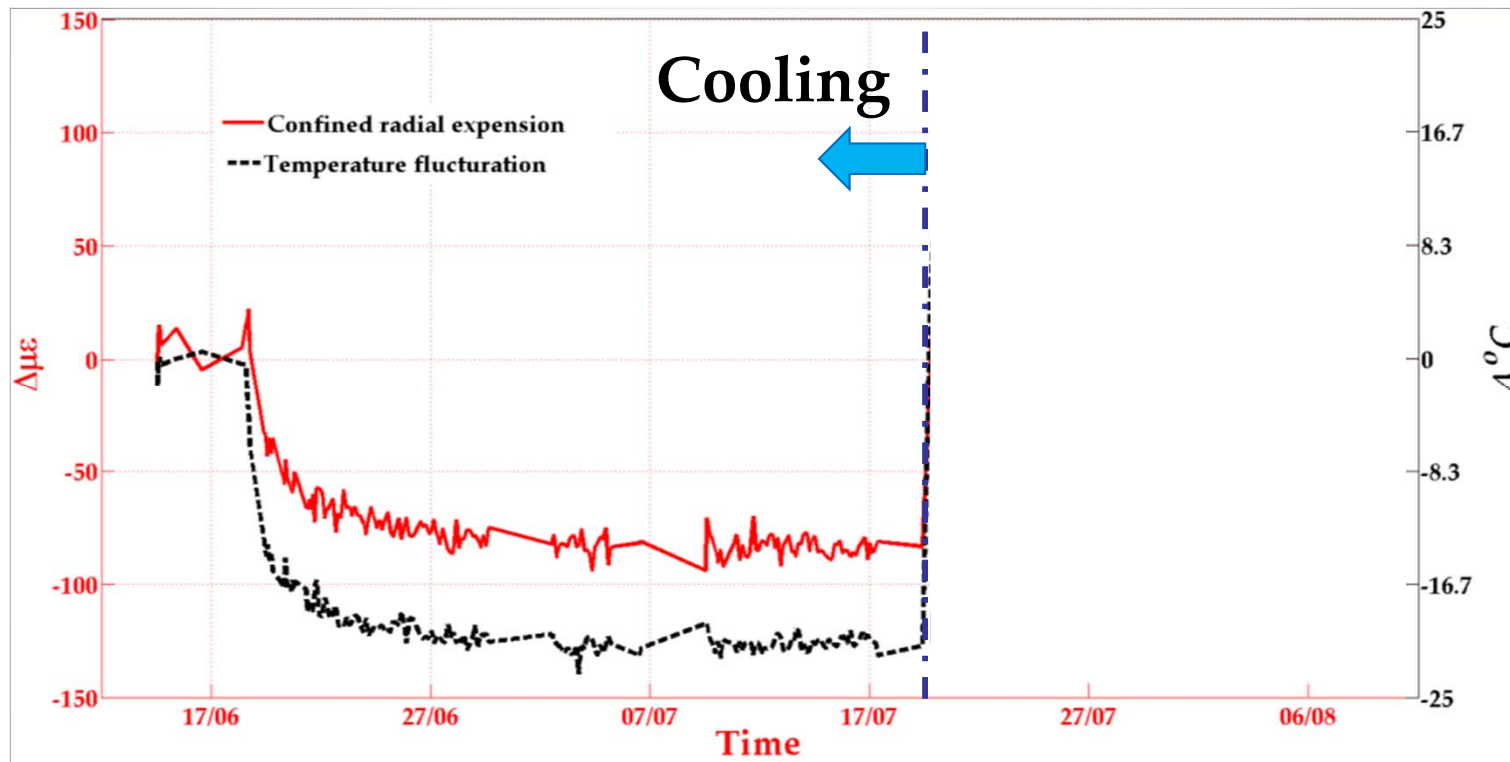
(ii) Heating, $\Delta T = +10^\circ\text{C}$

Check 1: Is the stress in the concrete smaller than the strength?



Thermal stress in heating > Thermal stress in cooling. Why?

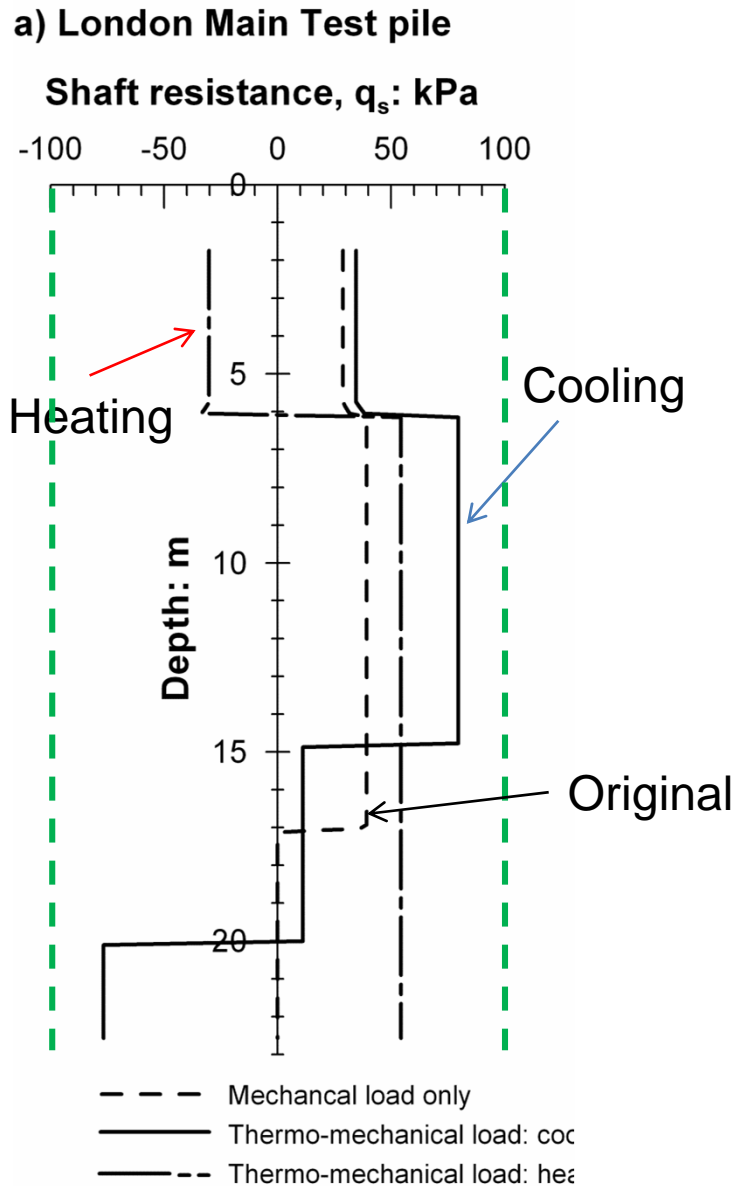
Measurement of radial strain



A bigger diameter pile will have more radial displacement

What is the effect on heat transfer and shaft resistance?

Check 2&3: Are the mobilised shaft friction and the end bearing pressure smaller than the design limits?



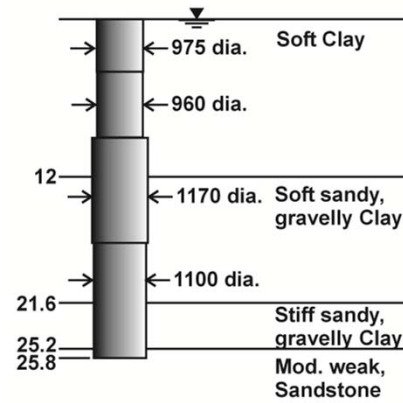
But....

No change in ultimate strength?

Cyclic heating and cooling will damage the clay?

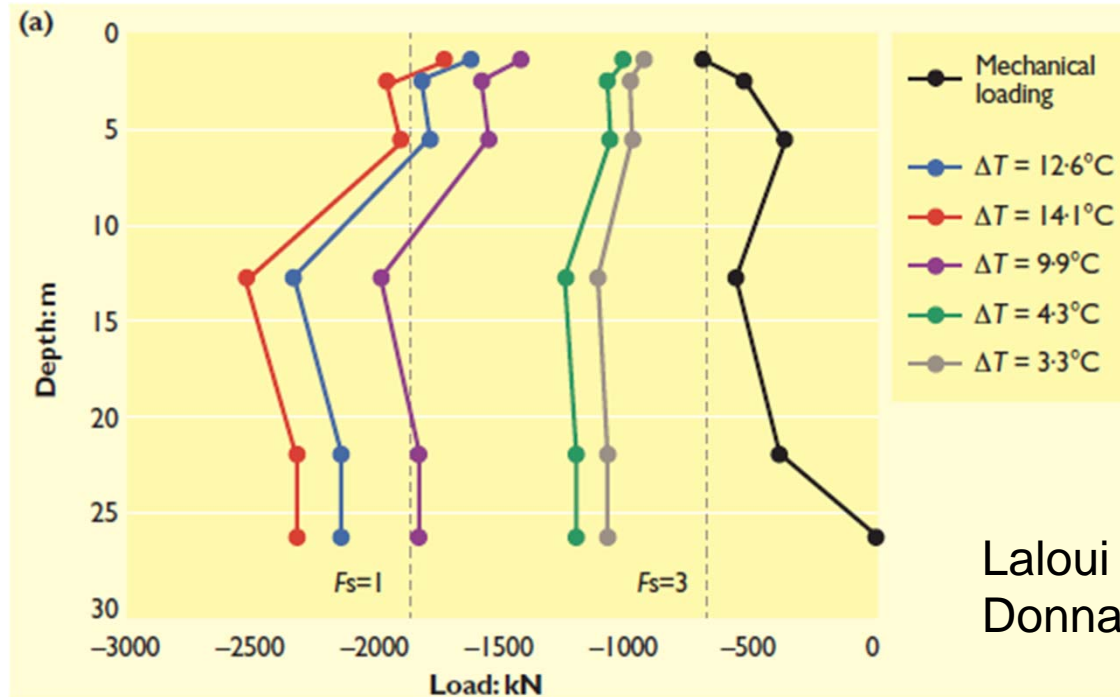
Short term test (with excess pore pressure) versus long-term performance (excess pore pressure dissipation)

b) Lausanne



Typical soil properties

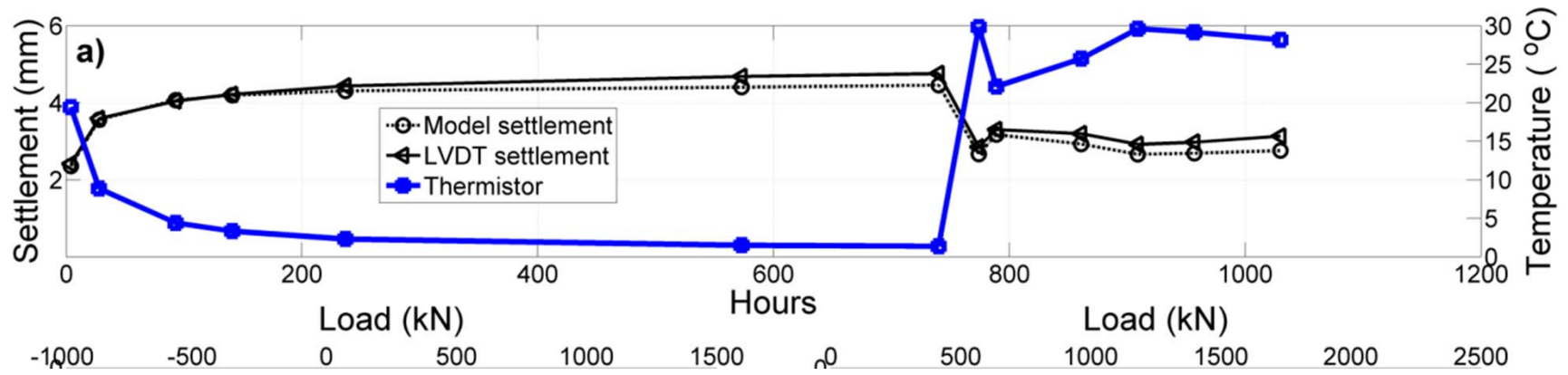
Soft Clay	$\gamma = 19.6 \text{ kN/m}^3$ $c_u = 15 - 20 \text{ kPa}$
Soft sandy, gravelly Clay	$\gamma = 19.1 \text{ kN/m}^3$ $c_u = 20 - 30 \text{ kPa}$
Stiff, sandy gravelly Clay	$\gamma = 21.6 \text{ kN/m}^3$ $c_u = 70 - 150 \text{ kPa}$
Mod. weak Sandstone	$\gamma = 25 \text{ kN/m}^3$ UCS = 12 MPa



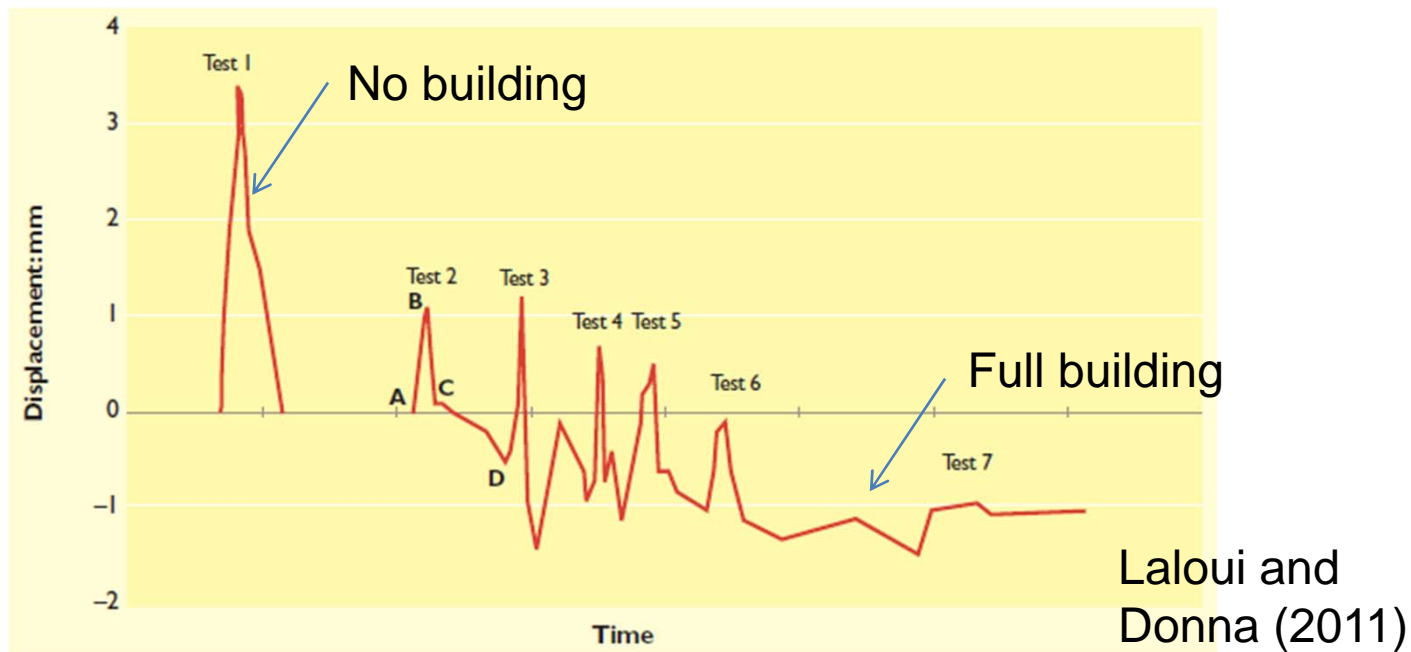
2400 kN load at the base is about 3 MPa

Check 4: Is the pile movement acceptable?

Lambeth College



EPFL Lausanne

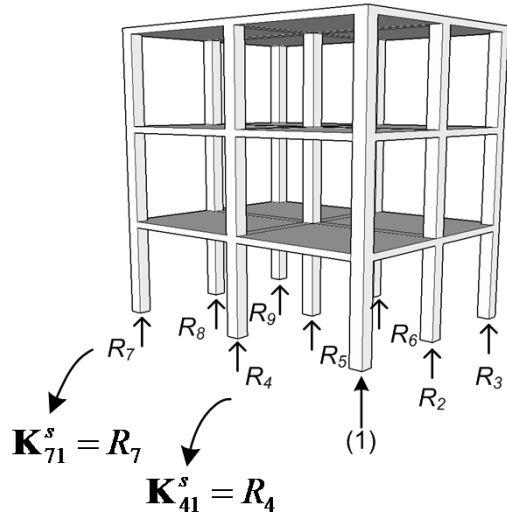


Laloui and Donna (2011)

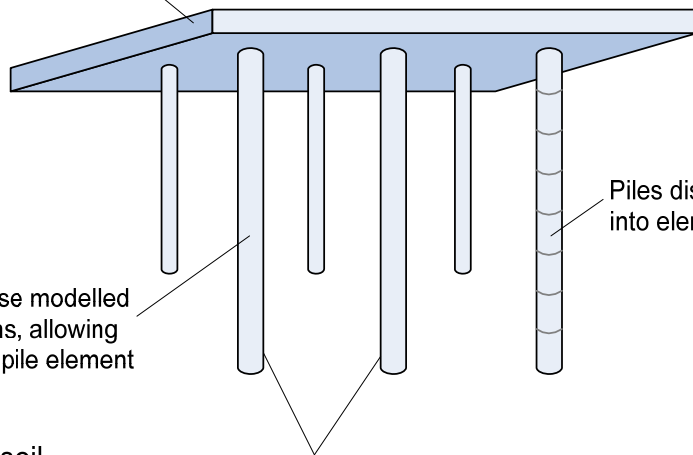
Thermal pile design software

↑ - Reaction at fixed node

↑ - Unit displacement at the node



Raft/cap discretised into four-node elements, modelled by FE (\mathbf{K}^r) method

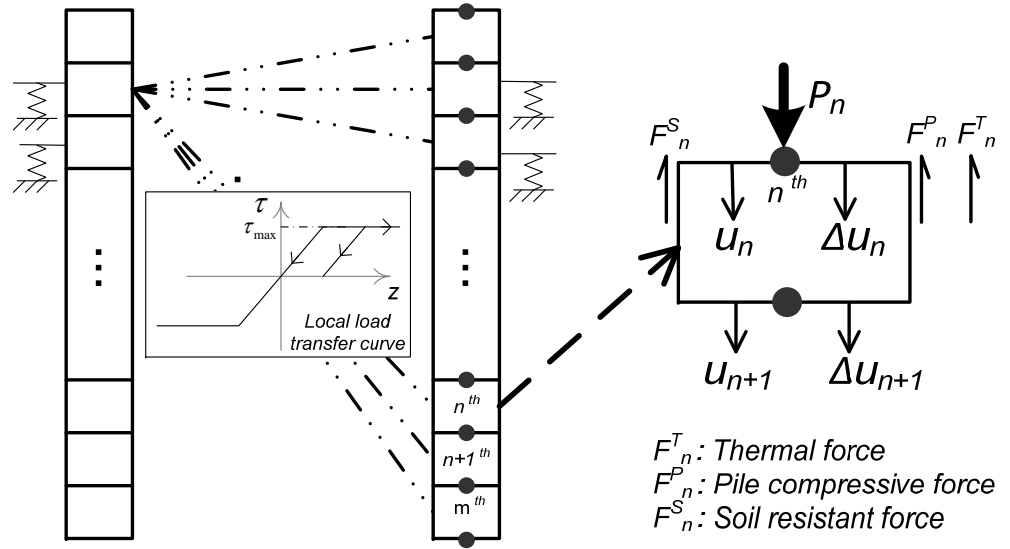


Piles discretised into elements (\mathbf{K}^p)

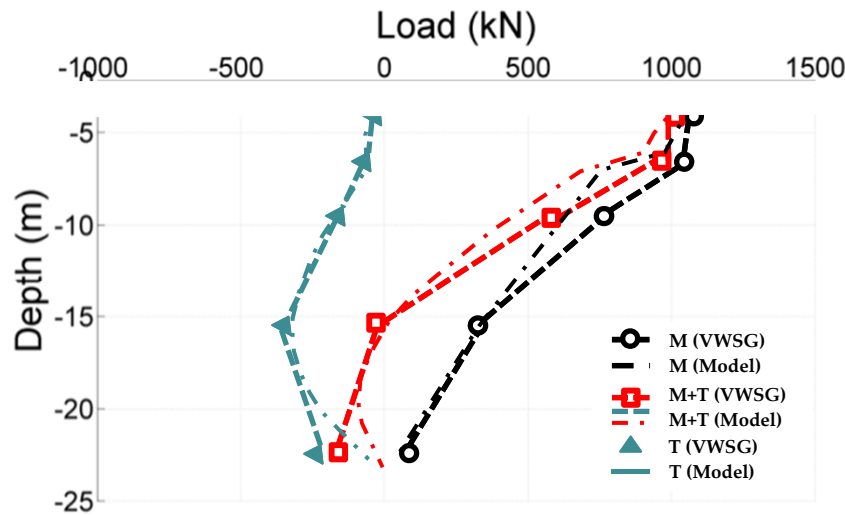
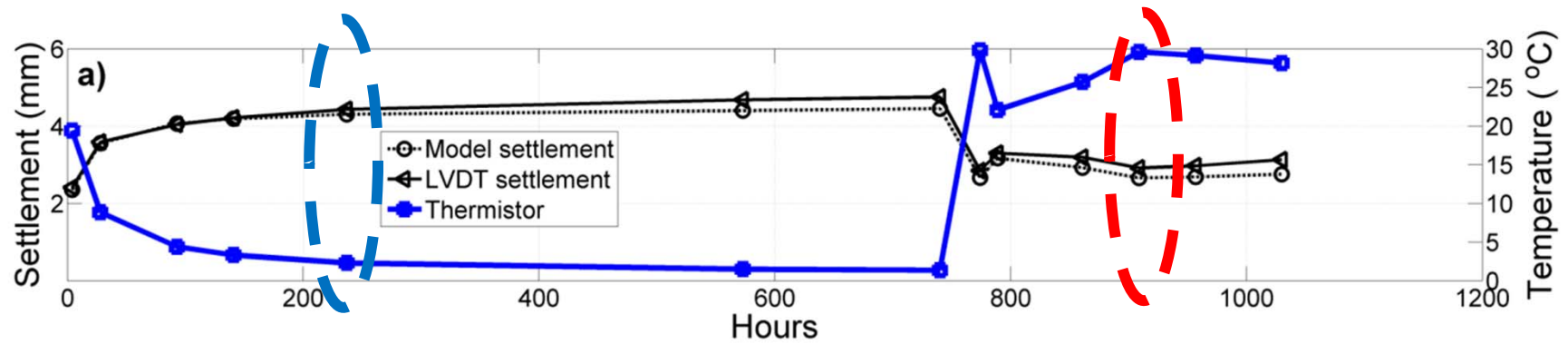
Individual pile response modelled by continuum solutions, allowing slip between soil and pile element if capacity is reached

(\mathbf{K}^{soil})

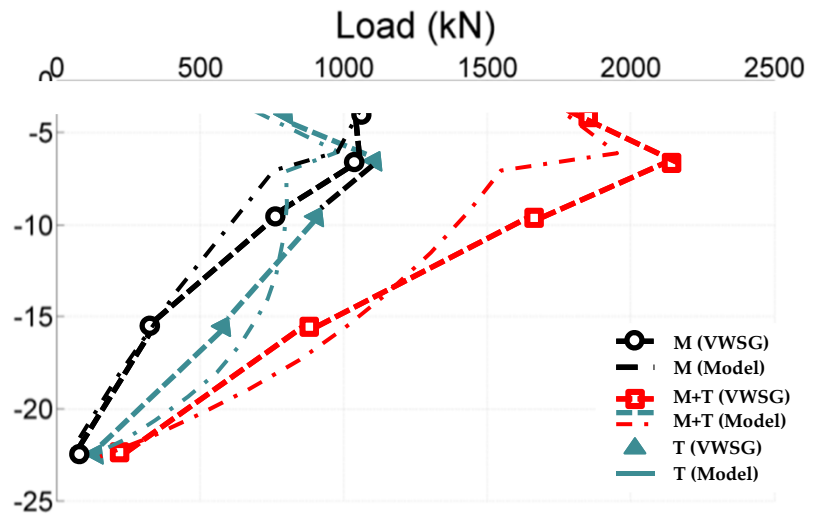
Pile-to-pile and pile-raft interaction evaluated by elastic solutions



Results

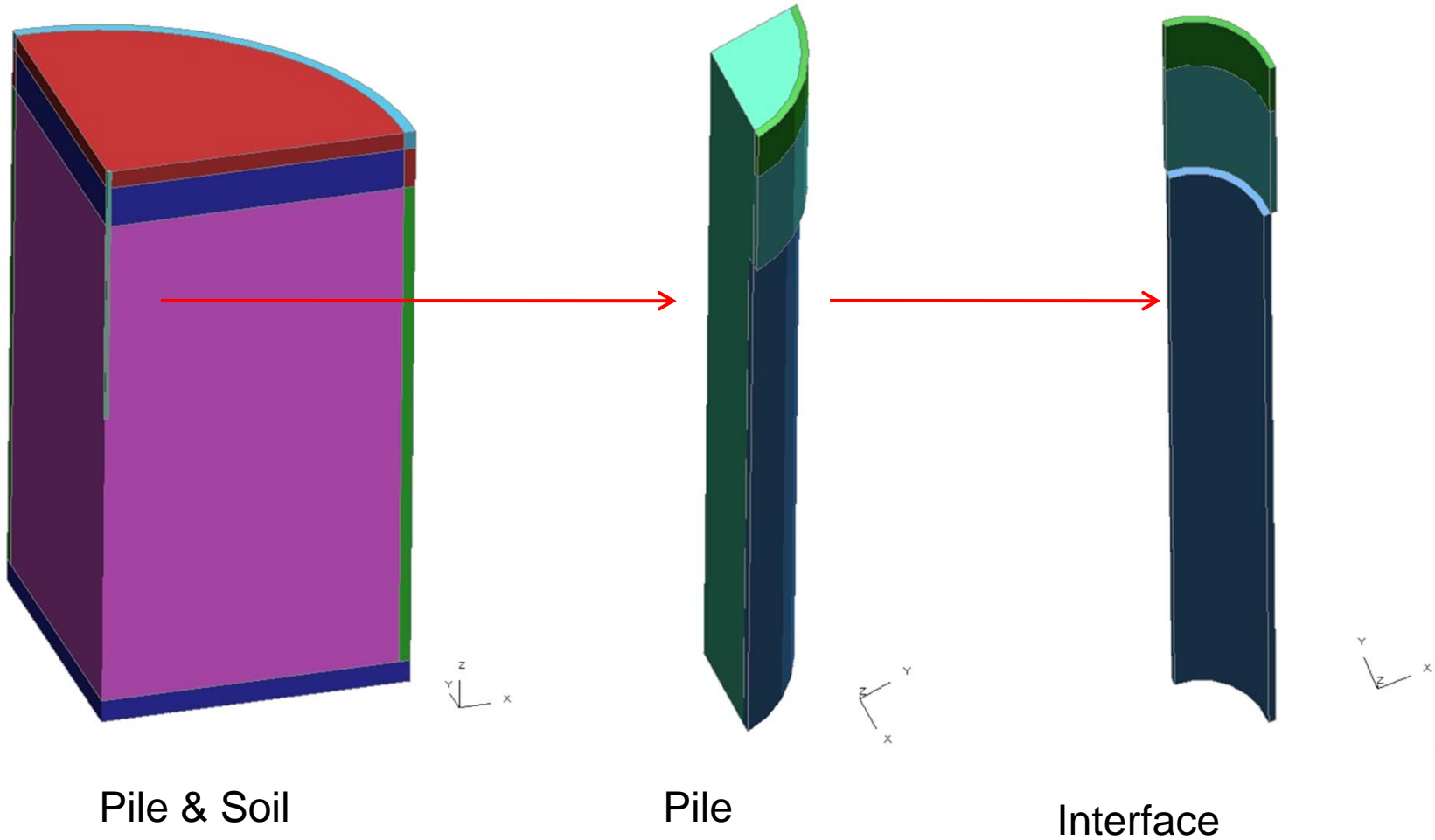


Cooling: $E_s = 450 * C_u$

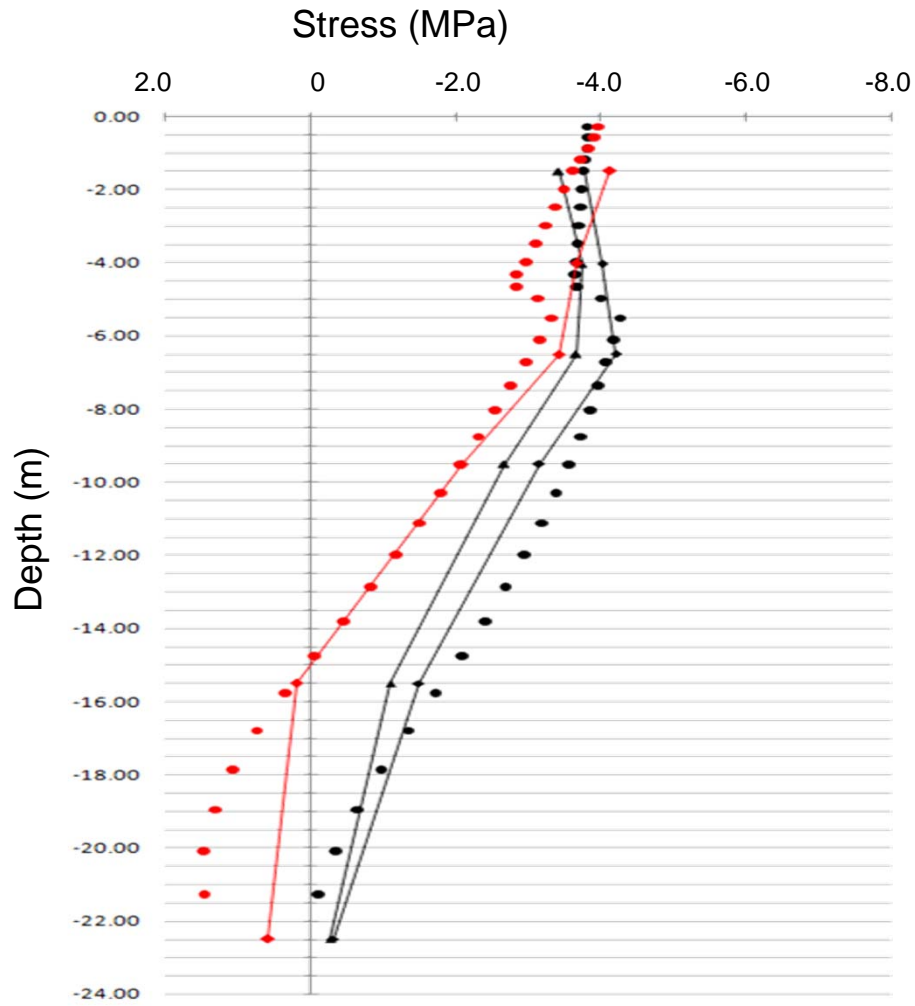


Heating: $E_s = 600 * C_u$

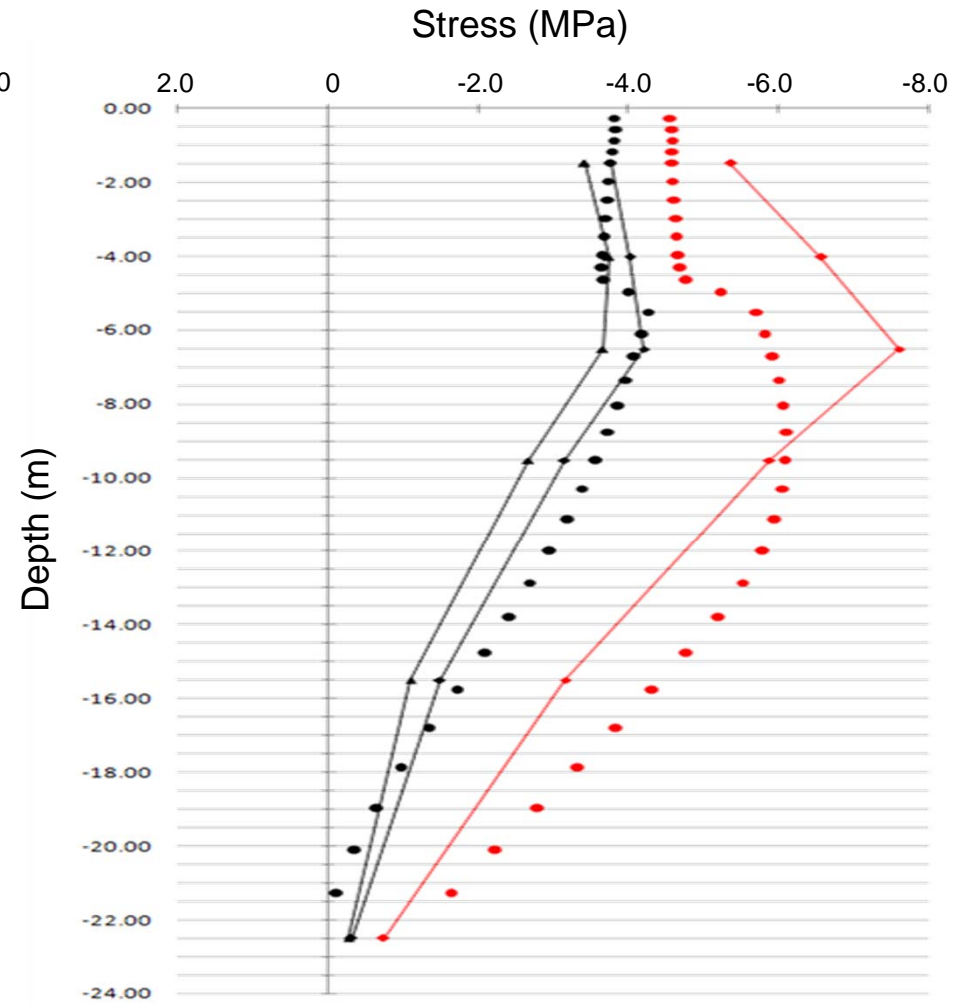
Finite Element Analysis of Thermal Pile



End of Cooling



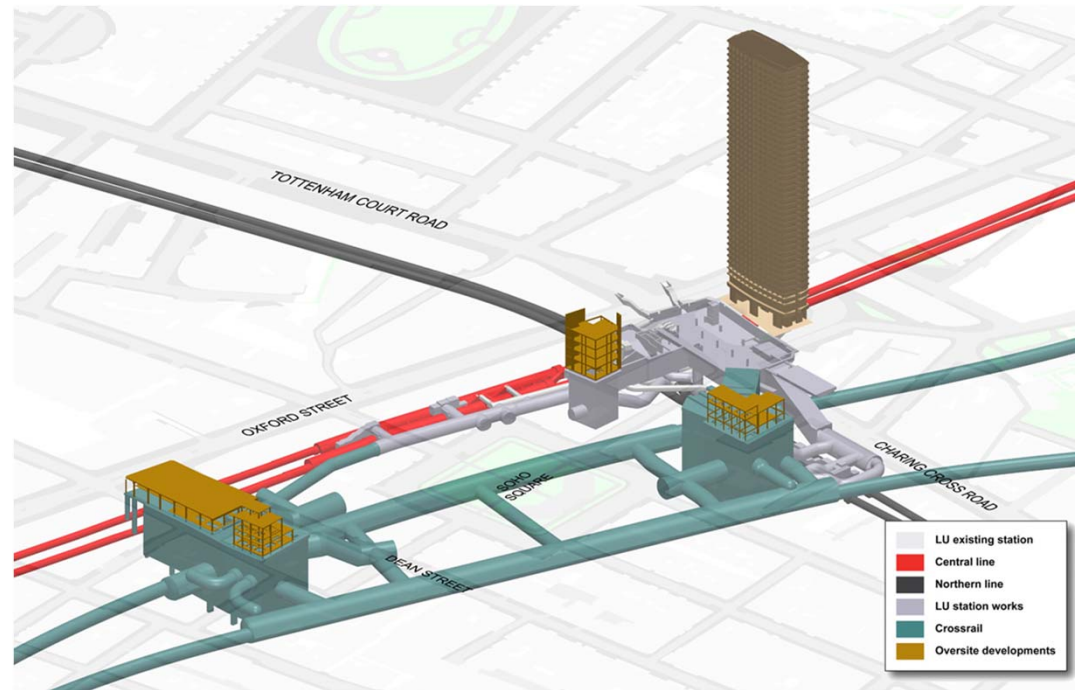
End of Heating



Summary for Thermal Piles

- **Check 1: Stress in the concrete is less than the allowable limit.**
 - Extreme – assume that the pile is fully restrained.
- **Check 2: Mobilised shaft friction is less than the design limit.**
 - Assume that the pile can fully expand at both ends but no movement at somewhere in the middle?
- **Check 3: End bearing pressure is less than the design limit.**
 - Extreme – assume that the pile is fully restrained. But end movement will reduce the thermally applied load.
- **Check 4: Pile movement is less than what the superstructure can tolerate.**
 - Need to do pile-soil interaction analysis

Thermal Walls – extracting heat from “hot” station



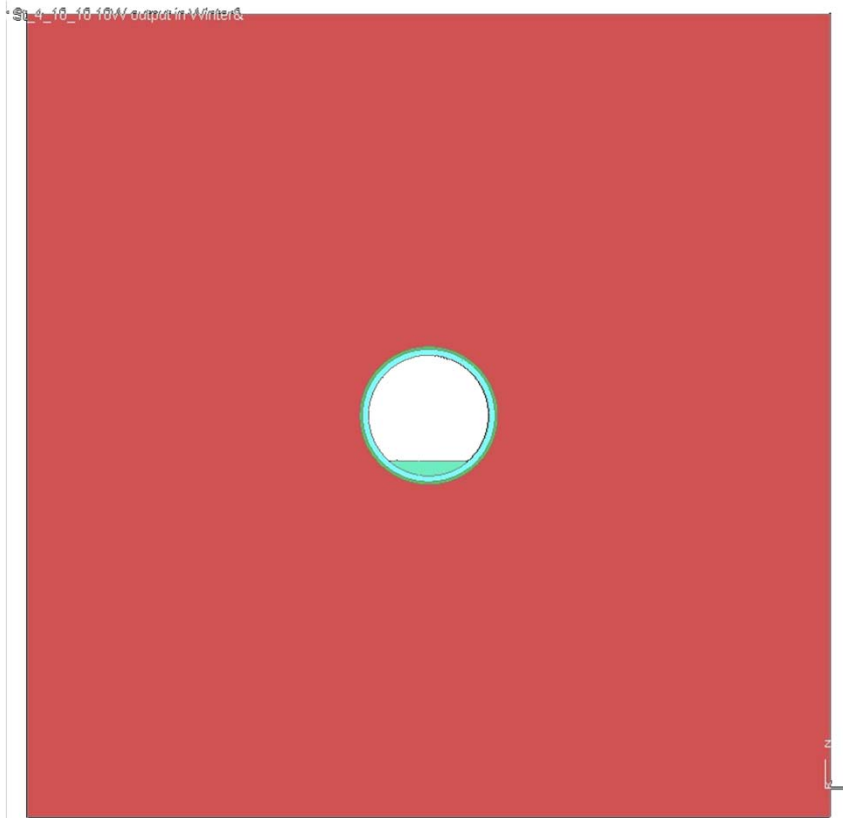
Tottenham Court Station



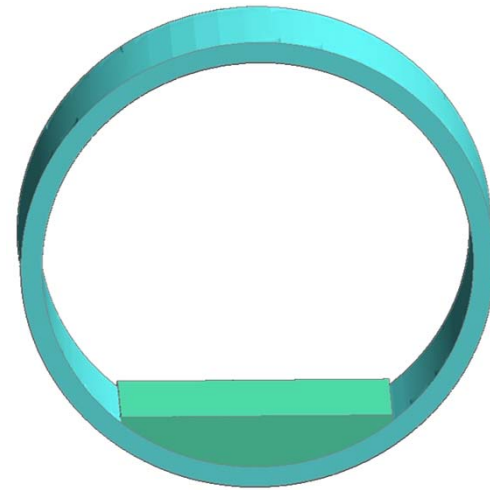
Wall bending?

Soil expansion – increase in earth pressure? Strut loads?

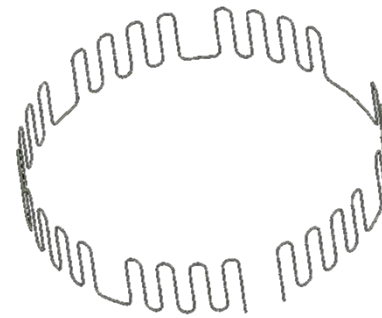
Thermal Tunnels – extracting heat from ‘hot’ tunnels



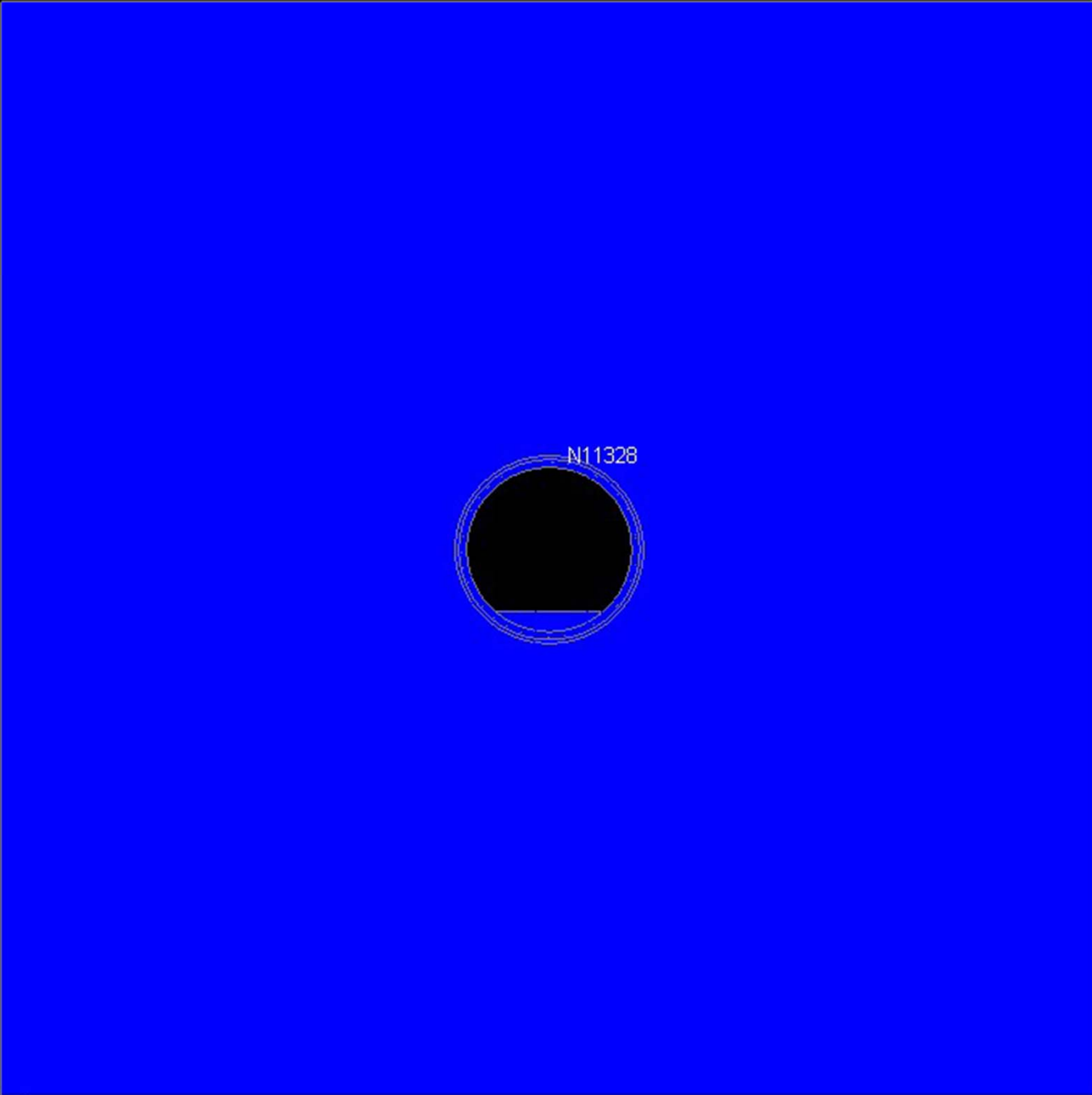
Whole Model



Tunnel Segment



Pipe



14.80

16.31

17.82

19.32

20.83

22.34

23.85

25.35

26.86

28.37

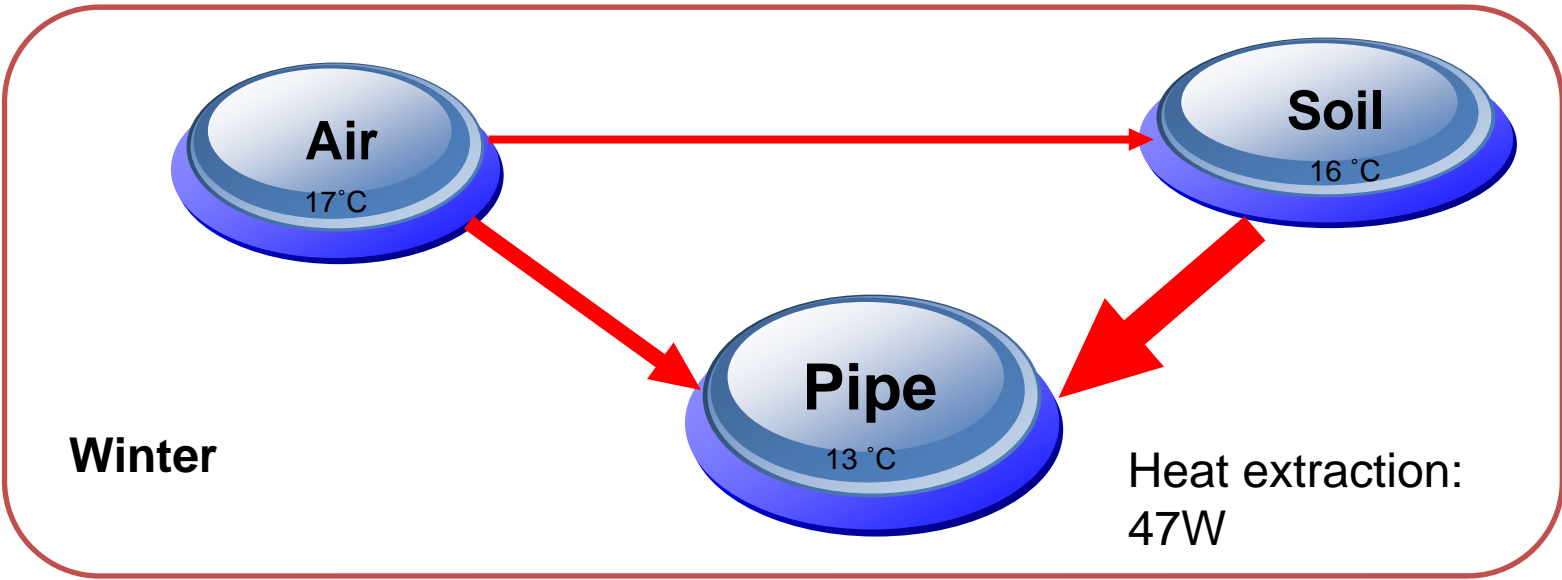
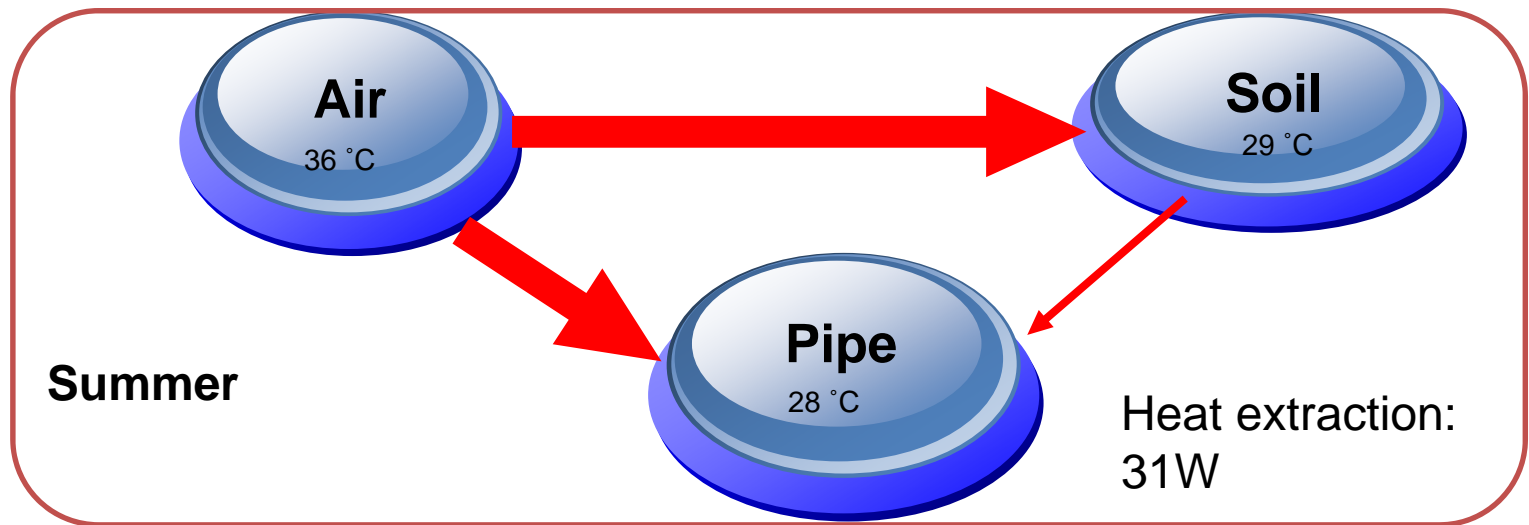
29.88

31.39

32.89

34.40

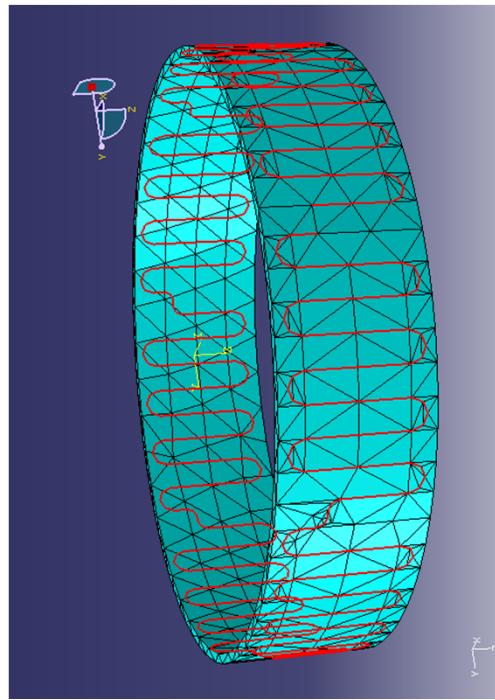
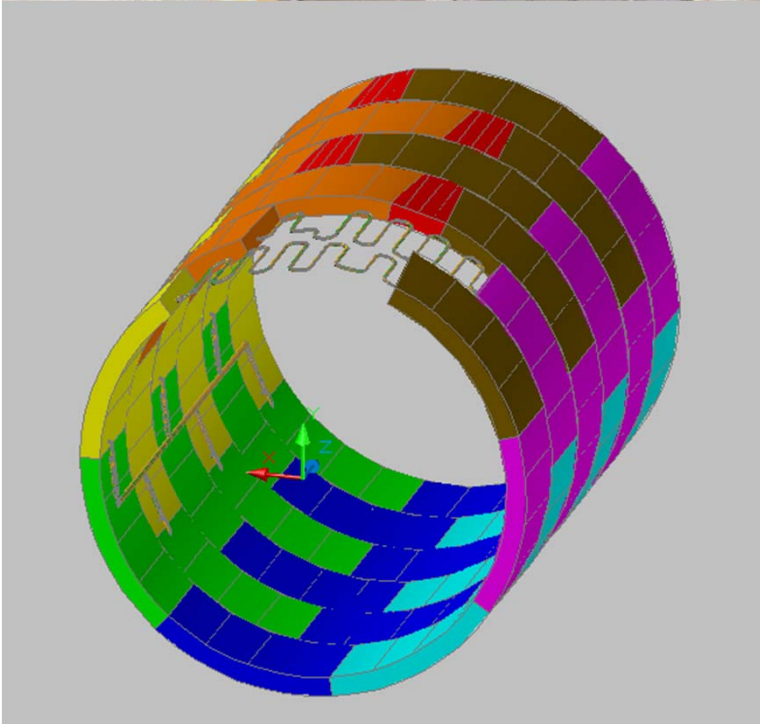
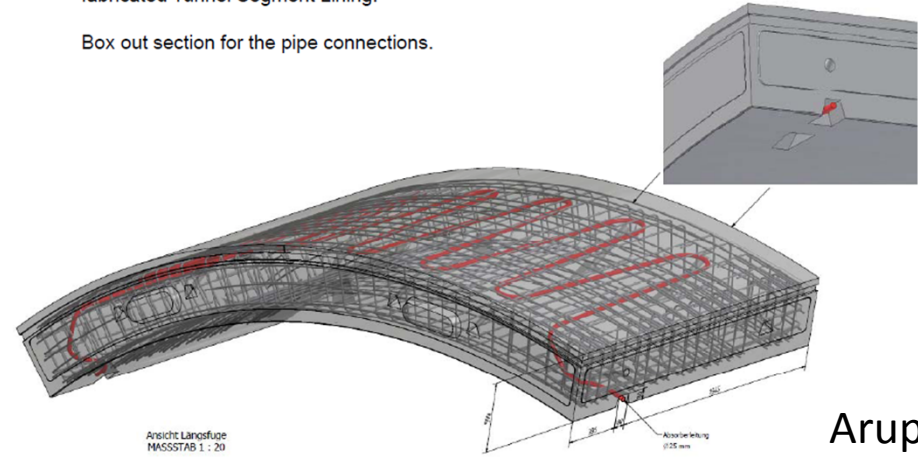






Positioning of the absorber pipe inside the pre-fabricated Tunnel Segment Lining.

Box out section for the pipe connections.



Lining stresses?

Final remarks

- Appreciation of the difference between “External” loading versus “Internally” generated thermal loading.
- We now know better, but more questions to be answered because of this.
- Opportunities and Challenges in thermal walls and thermal tunnels.

Thank you.